



# Cloich Forest Wind Farm

Volume 3 – SEI Report Technical Appendices  
(Part 1 of 2)

November 2022



# CLOICH FOREST WIND FARM

## SEI Report – Volume 3 – SEI Report Technical Appendices (Part 1 of 2)

**A6.1** Post Application Consultation with Historic Environment Scotland

**A9.1** Peat Slide Risk Assessment

**A9.2** Outline Peat Management Plan





# ARCUS

**CLOICH FOREST WIND FARM**

**VOLUME 3: SEI REPORT TECHNICAL  
APPENDICES**

**TECHNICAL APPENDIX A6.1: POST  
APPLICATION HISTORIC  
ENVIRONMENT SCOTLAND  
CONSULTATION**

**NOVEMBER 2022**



Prepared By:

**Arcus Consultancy Services**

7th Floor  
144 West George Street  
Glasgow  
G2 2HG

**T** +44 (0)141 221 9997 | **E** [info@arcusconsulting.co.uk](mailto:info@arcusconsulting.co.uk)  
**w** [www.arcusconsulting.co.uk](http://www.arcusconsulting.co.uk)

Registered in England & Wales No. 5644976



Ms Ruth Cameron  
Historic Environment Scotland

11 November 2021

Your Ref: 300039684  
Planning Ref: ECU00003288

Dear Ms Cameron

## **Proposed Cloich Forest Wind Farm: Applicant Response to HES Objection**

### **Overview**

Thank you for your recent consultation response regarding the proposed Cloich Forest Wind Farm ('the Development'). On behalf of EDF Renewables / Cloich Windfarm Partnership LLP ('the Applicant'), Arcus Consultancy Services Ltd (Arcus) seeks to respond to Historic Environment Scotland (HES) by outlining recent changes in relation to the Development turbine layout design.

In HES's consultation response, dated 16 September 2021, an objection was lodged due to setting impacts, caused by T8, on Whaup Law Cairn, designated as a scheduled monument (SM2755). HES noted in their response,

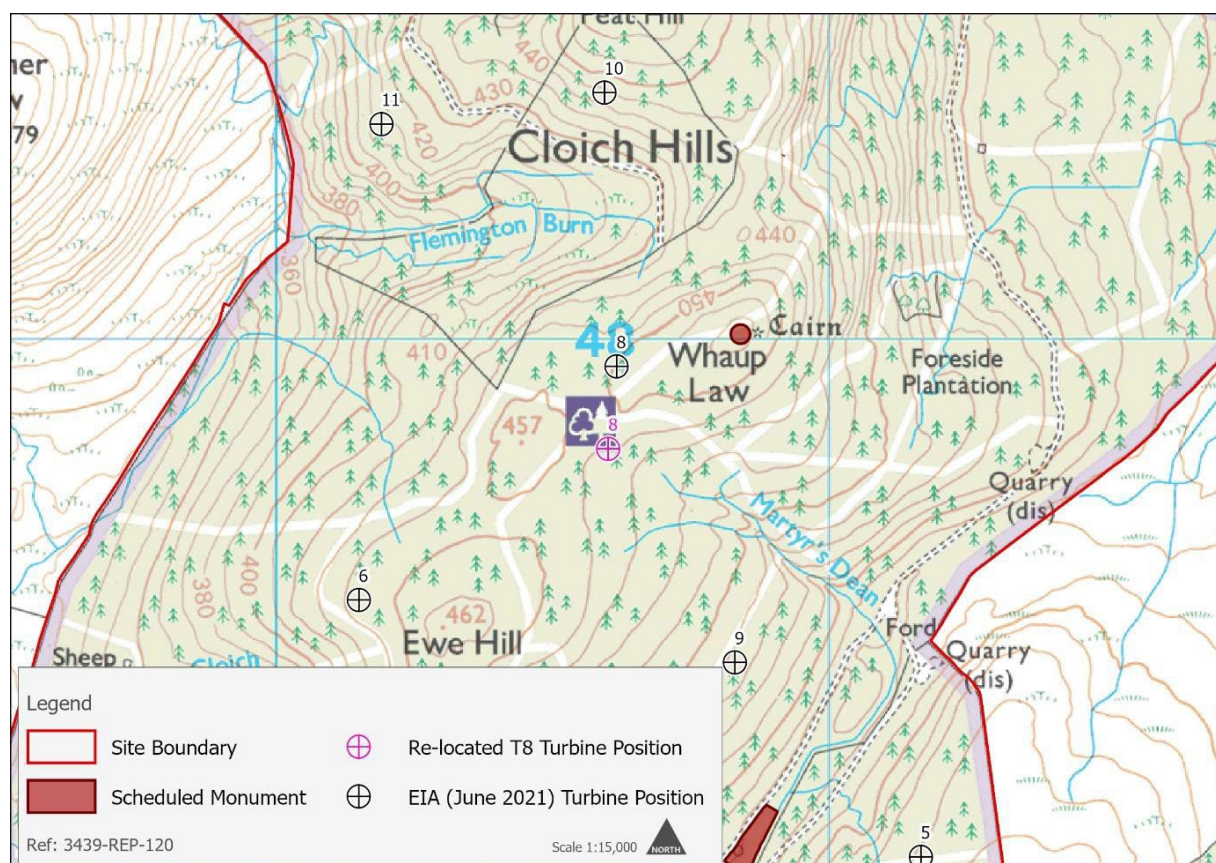
*"...that a limited alteration to the scheme would be sufficient to allow us [HES] to withdraw our objection..."*

### **Applicant Response & T8 Relocation**

The Applicant, advised by Arcus archaeology and cultural heritage experts, has investigated relocating T8 in light of the advice from HES. The relocation of T8 was made in consultation with various other environmental and engineering experts to ensure other site constraints were not unduly compromised.

The EIA application location for T8 was National Grid Reference (NGR) 320616, 647950 – located approximately 200 m west-southwest of SM2755. Following consideration of the HES response, and the setting impact of the original T8 location, the new proposed location for T8 is NGR 320601, 647801 – located approximately 300 m southwest of SM2755. Plate 1, overleaf, illustrates the original and new location of T8.

## Plate 1: T8 Relocation



The alternative location for T8 represents a ~150 m southward move from its original location; the movement takes T8 down 10 m Above Ordnance Datum (AOD) from 450 m AOD to 440 m AOD, and off of the crest of the hill on which SM2755 lies. Further movement south is constrained by a deposit of deep peat (currently avoided), as well as other environmental/technical considerations including:

- Increased slope;
- Landscape and visual impacts;
- Turbine spacing; and
- Close proximity to 50 m watercourse buffers.

Appendix A contains four wirelines<sup>1</sup>, as follows:

- **Figure A1:** SM2755 Whaup Law Cairn T8 Comparison (180 degree field of view);
- **Figure A2:** SM2755 Whaup Law Cairn T8 Relocation (180 degree field of view);
- **Figure A3:** SM2738 Whether Law Cairn T8 Comparison (120 degree field of view); and
- **Figure A4:** SM2738 Whether Law Cairn T8 Relocation (120 degree field of view).

Figures A1 & A3 provide a comparative Wireline showing the Development with both the original and relocated T8, with the wider Development layout. Figures A2 & A4 provide a wireline showing the revised layout for the Development.

In the original location, it is acknowledged that, whilst not within the direct sightline from Whaup Law Cairn to Whether Law Cairn, T8 is within close proximity to SM2755. **Technical Appendix A6.3: Setting Assessment of Chapter 6: Archaeology & Cultural Heritage** of the EIA

<sup>1</sup> The wirelines provided are illustrative only and not produced in accordance with current NatureScot visualisation guidance.

Report submitted in support of the Section 36 Application ('the Application') for the Development, concluded that,

*"Whilst there would still be commercial forestry on the slopes of Whaup Law surrounding the monument, the height of the turbines would change the appreciation and experience of the monument with the benefit of a more open setting around the cairn but within the context of a modern wind farm. On balance, the magnitude of change to the cultural significance is considered moderate."*

Consequently, a significant effect in terms of the EIA Regulations<sup>2</sup> was concluded for SM2755.

Through the relocation of T8 the proposed turbine position is now a further 100 m away (300 m in total) from the scheduled monument and located further south. Figures A1 to A4 show that the relocated T8 would be further away from the cairn and less prominent, as it no longer shares the hill summit with the monument. This is a marked improvement to the layout, enabling Whaup Law Cairn to be the dominant feature upon the hill top with the turbines a slightly more distant and separate component visible above the forestry treeline. The relocation to the south-west has also increased the gap between T8/T6 to the south and T11 to the north so that there is a wider field of view / viewshed available between Whaup Law and Wether Law Cairns as shown in Figures A1 & A2.

### **Conclusion**

It is hoped that the above relocation of T8 and the information provided, combined with the information previously provided in the Application, addresses the concerns that HES identified. I would be grateful if you could consider the information that we have provided and let us know if the alternative location would enable HES to remove its objection. If so, it will be necessary for the Applicant to formally propose this new location and present updated information in the form of Supplementary Environmental Information (SEI) which would include additional ground investigation data for the realignment of tracks and relocation of the turbine. We would be grateful for your feedback prior to this work being commissioned.

Should HES require any further information, please contact me on the details below to discuss; Arcus would be happy to arrange a meeting or call if that would be helpful.

Yours sincerely,

**Heather Kwiatkowski (MCIfA)**

**Principal Consultant (Archaeology & Cultural Heritage)**

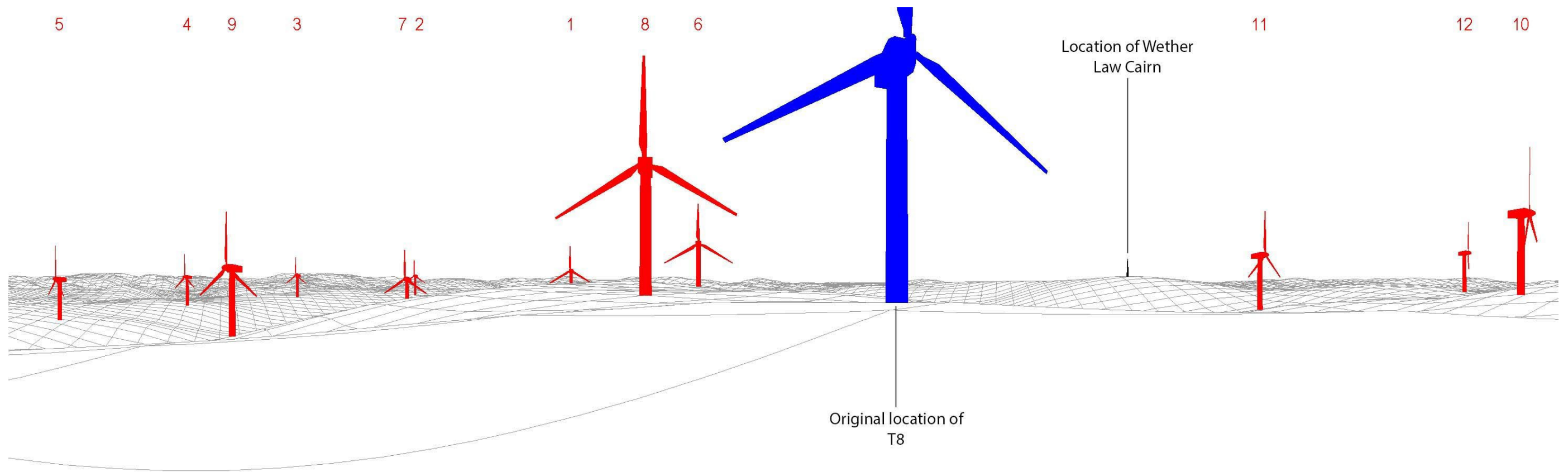
---

<sup>2</sup> The Electricity Works (Environmental Impact Assessment) (Scotland) Regulations 2017. [Online] Available at: <http://www.legislation.gov.uk/ssi/2017/101/contents/made> (Accessed 08/11/2021)

## **Appendix A**

### **Figure A1: SM2755 Whaup Law Cairn T8 Comparison (180 degree field of view)**





SM2755 Whaup Law Cairn

Figure A1: SM2755 Whaup Law Cairn T8 Comparison (180 degree field of view)

**Figure A2: SM2755 Whaup Law Cairn T8 Relocation (180 degree field of view)**

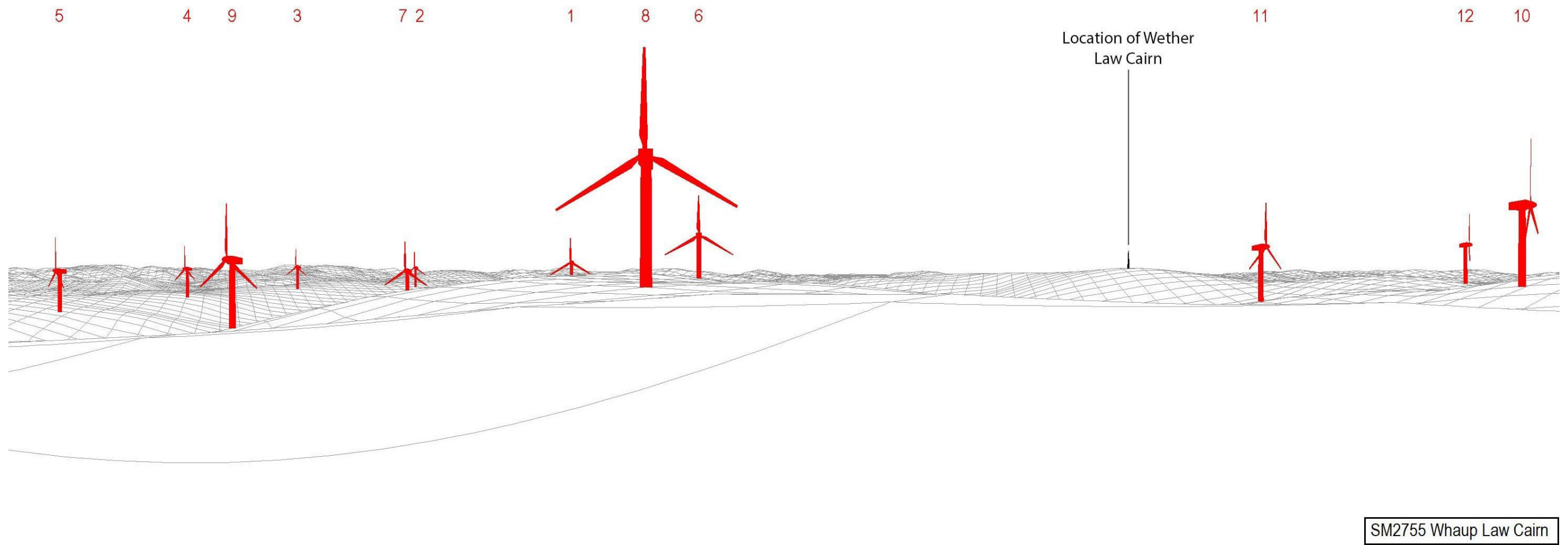
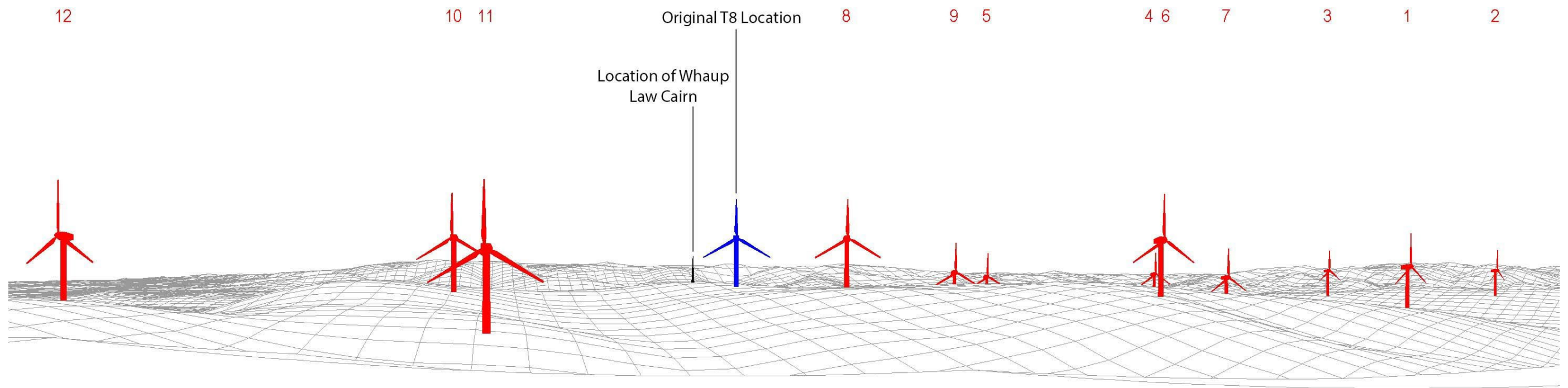


Figure A2: SM2755 Whaup Law Cairn T8 Relocation (180 degree field of view)

**Figure A3: SM2738 Whether Law Cairn T8 Comparison (120 degree field of view)**



SM2738 Wether Law Cairn

Figure A3: SM2738 Whether Law Cairn Comparison (120 degree field of view)

**Figure A4: SM2738 Whether Law Cairn T8 Relocation (120 degree field of view)**

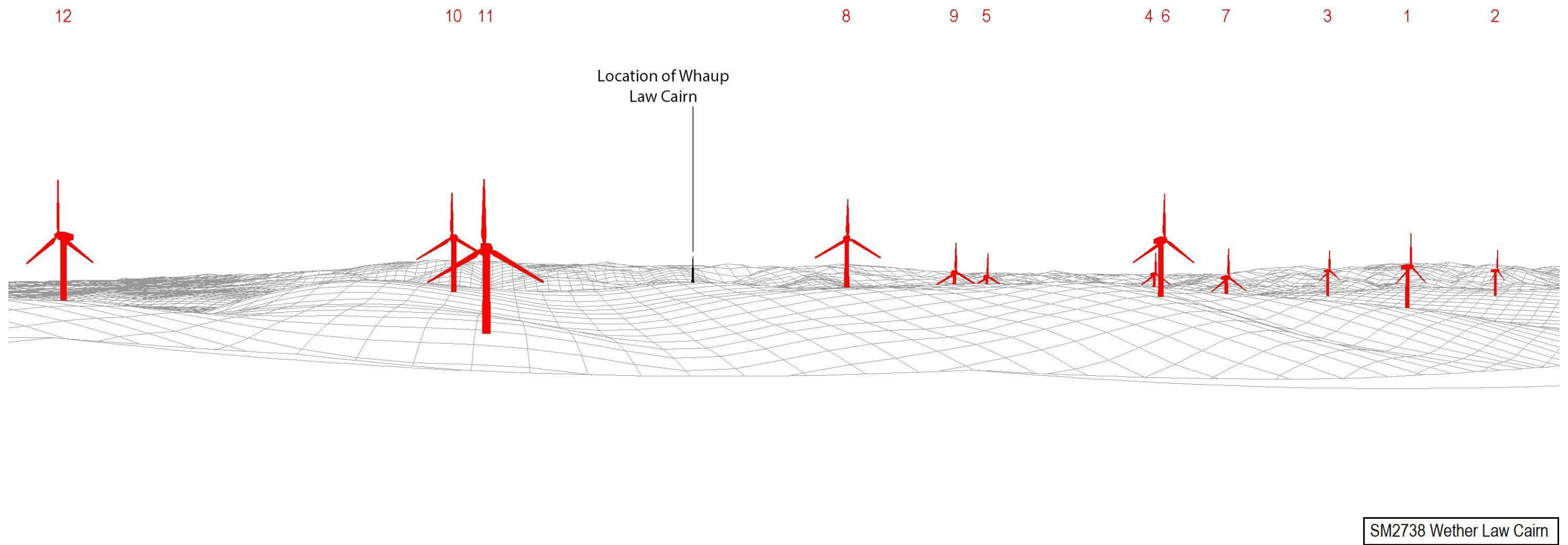


Figure A4: SM2738 Whether Law Cairn Relocation (120 degree field of view)

**From:** [Ruth Cameron](#)  
**To:** [Fraser Clarke](#)  
**Cc:** [Richard Fisher](#); [Heather Kwiatkowski](#); [Fiona MacGregor](#); [Debbie Flaherty](#); [Deirdre Cameron](#)  
**Subject:** RE: Cloich Forest Wind Farm: T8 Relocation Consultation  
**Date:** 03 December 2021 10:40:33  
**Attachments:** [image005.png](#)  
[image006.png](#)  
[image007.png](#)  
[image008.jpg](#)  
[image001.png](#)  
[image002.png](#)  
[image003.png](#)  
[image004.png](#)  
[image009.png](#)

---

Fraser,

We have done an initial review of the changes to the scheme. While we can't get offer you a detailed commentary at the moment, I thought it best to give you our expected position, so that you can continue to progress the proposals.

The relocation of turbine 8 as demonstrated in your consultation should allow us to remove our objection to the scheme, based on the information we have available. The new location proposed for Turbine 8 is similar to that of Turbine 9 of the previous (consented) scheme; a little higher in elevation and taller, but slightly further way from the monument. The potential setting impacts on the cairn from the current proposal are therefore likely to be very similar to that from the earlier consented scheme. We do not consider this impact to raise issues in the national interest and therefore would not object to the revised proposals.

Please note that this is not a formal statement of our position. We will give this in full if and when we are consulted by ECU on this variation. However, we expect this to be our position based on the current information.

We hope that this is helpful to you as you continue to work on the proposals. And we hope to be able to formalise this position at a later date.

Kind regards,  
Ruth

**Ruth Cameron | Senior Environmental Assessment and Advice Officer | Planning, Consents and Advice Service**

**Pronouns: she/her**

*We inform and enable good decision-making so that the historic environment of Scotland is valued and protected.*

Historic Environment Scotland | Àrainneachd Eachdraidheil Alba  
Longmore House, Salisbury Place, Edinburgh, EH9 1SH

[www.historicenvironment.scot](http://www.historicenvironment.scot)

**[Heritage For All - read our new Corporate Plan and help to share our vision](#)**



---

**Sent:** 01 December 2021 09:54

**To:** Ruth Cameron

**Cc:** Richard Fisher; Heather Kwiatkowski; Fiona MacGregor ; Debbie Flaherty

**Subject:** RE: Cloich Forest Wind Farm: T8 Relocation Consultation

Hi Ruth,

Thanks for your email. I'm sorry to hear that you are unwell with covid – I hope it continues to be mild and that you recover soon. I've been lucky enough to avoid it so far – touch wood!

I would be grateful if you could advise us if your situation changes and it looks like you will be on leave for longer.

Thank you very much for updating us whilst you are unwell, it is very much appreciated.

Kind regards,

Fraser

---

**From:** Ruth Cameron

**Sent:** 01 December 2021 09:37

**To:** Fraser Clarke

**Subject:** RE: Cloich Forest Wind Farm: T8 Relocation Consultation

Fraser,

I just wanted to drop you a line as I know you're still awaiting a response on this. I'm afraid I'm actually currently sick with covid (not seriously ill, but i still wouldn't recommend it if you haven't tried it yet).

We don't have any available cover in the team so this will have to wait until I'm back at my desk. Which of course I'm hoping won't be too long but it is a bit uncertain at the moment.

I hope this isn't causing too much of a delay at your end. I hope to be able to answer fairly promptly once I'm back at work.

All the best,

Ruth

---

**From:** Fraser Clarke

**Sent:** 17 November 2021 14:48

**To:** Ruth Cameron

**Cc:** HM - Consultations; Debbie Flaherty; Richard Fisher ; Fiona MacGregor; Heather Kwiatkowski

**Subject:** RE: Cloich Forest Wind Farm: T8 Relocation Consultation

Dear Ruth,

I hope you are well. Apologies for my follow up email. The project team wanted to check with you that you received the below consultation regarding HES' objection to the proposed Cloich Forest Wind Farm.

The project team would be very grateful if you could confirm receipt of the below and, if possible, please advise on when HES might be able to respond.

Kind regards,  
Fraser

---

**From:** Fraser Clarke

**Sent:** 11 November 2021 13:35

**To:**

**Cc:** Richard Fisher; Fiona MacGregor; Heather Kwiatkowski

**Subject:** Cloich Forest Wind Farm: T8 Relocation Consultation

Dear Ruth,

I hope you are well.

Following email correspondence between HES and my colleague Heather Kwiatkowski (dated 6<sup>th</sup> - 7<sup>th</sup> October), please find attached consultation in respect of the proposed Cloich Forest Wind Farm (the Development) and a proposed relocation of T8. As detailed within the attached letter, it is hoped this relocation of T8 is sufficient for HES to remove their objection to the Development.

Should you have any questions regarding the attached, please do get in touch.

We look forward to HES's response.

Kind regards,  
Fraser

**Fraser Clarke**  
Environmental Consultant  
Arcus Consultancy Services Ltd

Web: [www.arcusconsulting.co.uk](http://www.arcusconsulting.co.uk)



ARCUS

**CLOICH FOREST WIND FARM  
SUPPLEMENTARY ENVIRONMENTAL INFORMATION**

**VOLUME 3: SEI REPORT TECHNICAL APPENDICES**

**TECHNICAL APPENDIX A9.1:  
PEAT SLIDE RISK ASSESSMENT**

**NOVEMBER 2022**



Prepared By:

**Arcus Consultancy Services**

7<sup>th</sup> Floor  
144 West George Street  
Glasgow  
G2 2HG

**T** +44 (0)141 847 0340 | **E** [info@arcusconsulting.co.uk](mailto:info@arcusconsulting.co.uk)  
**w** [www.arcusconsulting.co.uk](http://www.arcusconsulting.co.uk)

Registered in England & Wales No. 5644976

## TABLE OF CONTENTS

<b>1</b>	<b>INTRODUCTION .....</b>	<b>1</b>
<b>2</b>	<b>SITE INFORMATION AND DESK STUDY .....</b>	<b>3</b>
<b>3</b>	<b>GUIDANCE AND METHODOLOGY.....</b>	<b>7</b>
<b>4</b>	<b>SITE SURVEYS AND RESULTS.....</b>	<b>10</b>
<b>5</b>	<b>HAZARD AND EXPOSURE ASSESSMENT .....</b>	<b>12</b>
<b>6</b>	<b>HAZARD RANKING .....</b>	<b>18</b>
<b>7</b>	<b>SLIDE RISK AND MITIGATION.....</b>	<b>19</b>
<b>8</b>	<b>CONCLUSIONS.....</b>	<b>29</b>
	<b>APPENDIX A - FIGURES.....</b>	<b>30</b>
	<b>APPENDIX B - SITE PHOTOGRAPHS.....</b>	<b>31</b>
	<b>APPENDIX C – HAZARD RANK ASSESSMENT RECORDS.....</b>	<b>35</b>

## 1 INTRODUCTION

### 1.1 Background

Arcus Consultancy Services Ltd (Arcus) was commissioned by Cloich Windfarm Partnership LLP, wholly owned by EDF Energy Renewables Limited, ('the Applicant') to carry out a Peat Slide Risk Assessment (PSRA) for the amendments to the proposed Cloich Forest Wind Farm (the SEI Layout) located within the Cloich Forest in the Scottish Borders, centred at approximately (NGR) 320648, 647881, approximately 5.5 kilometres (km) north-west of Peebles ('the Site'). This Supplementary Environmental Information (SEI) Report provides further, and updated, environmental information in light of revisions to the Development. The Applicant has revised the Development by:

- Relocating Turbine 8 (T8) and its associated infrastructure to ensure that it is sufficiently removed from Whaup Law Cairn;
- Provision for an additional control building at the substation compound. It is expected that the grid operator (SPT) will request a separate control building to the wind farm's control building.
- The addition of a new SPT Temporary Construction Compound (TCC) in the north of the Site.

Additional felling is required due to these changes. The SEI Layout is illustrated in Figure 9.1.1 within Appendix A of this PRHA and will consist of the following key infrastructure with changes incorporated within the SEI Layout shown in bold:

- Up to 12 wind turbines three-bladed turbines, **including the relocation of T8 150 m to the south**, with a maximum tip height of up to 149.9 m;
- Widening works along public roads 'D17 Whim – Shiplaw' & 'D18 Cloich';
- Access tracks linking the turbine locations;
- Network of underground cabling running adjacent to the access tracks where possible;
- Substation compound incorporating **two** single storey control **buildings**, external electrical infrastructure, BESS components, recycling and storage, and vehicle parking etc.;
- Crane hardstandings and an external transformer for each turbine;
- Temporary Construction Compound (TCC);
- Two Borrow Pits;
- **Scottish Power Transmission (SPT)TCC;**
- An approximate 20 MW battery energy storage system (BESS); and
- Forestry felling, **including an additional area required due to the relocation of T8** and additional TCC.

The PSRA supports **Chapter 9: Geology, Ground Conditions and Peat** of the SEI Report.

The PSRA is accompanied by the following appendices:

- Appendix A: Figures;
- Appendix B: Site Photographs; and
- Appendix C: Hazard Rank Calculations.

### 1.2 Scope and Purpose

The scope of this PSRA is to consider the SEI layout (T8 relocation and addition of a TCC) and address points raised by Ironside Farrar in the EIA application. This will be done in line with the following:

- Review available desk-based information on the Site;

- Undertake a site walkover survey and peat probe surveys to characterise the prevailing ground conditions and identify existing or potential peat instability;
- Report on the findings of the survey, assess the potential instability risk and estimate the hazard from any potential peat slide; and
- Recommend mitigation measures and specific construction methodologies that should be considered during the construction period, if required.

This PSRA provides factual information on the peat survey results relating to the Development. Desk-based information and site surveys have been utilised to assess the potential risk of any peat landslide. The methodology adopted and details on the assessment are outlined in Sections 3, 4 and 5. The assessment has been undertaken in accordance with Scottish Government Guidance<sup>1</sup> in assessing the likelihood and consequence of such an event.

The PSRA has been prepared by suitably qualified engineers, ecologists, and hydrologists at Arcus as shown in table 1.1 below.

Table 1.1: Author qualifications

<b>Team Member</b>	<b>Job Title</b>	<b>Qualifications</b>	<b>No. Years' Experience</b>
Gregor Hirst	Senior Engineer	BSc (Hons)	6 Years
David Ballentyne	Principal Engineer	BSc (Hons)	18 Years
Tomos Ap Tomos	Technical Director	BEng (Hons) MCIHT	25 Years

This assessment was undertaken by Gregor Hirst (BSc Hons), a Geo-Environmental Engineer of 6 years, and was supported by David Ballentyne a Geo-Environmental Civil Engineer with over 18 years of experience in ground condition assessment. This Chapter has been technically reviewed by Tomos Ap Tomos, Technical Director of Engineering.

<sup>1</sup> Scottish Government (2017) Peat Landslide Hazard and Risk Assessments: Best Practice Guide for Proposed Electricity Generation Developments (Accessed 10/10/22) Available at: <https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2017/04/peat-landslide-hazard-risk-assessments-best-practice-guide-proposed-electricity/documents/00517176-pdf/00517176-pdf/govscot%3Adocument/00517176.pdf>

## **2 SITE INFORMATION AND DESK STUDY**

### **2.1 Site Description and Topography**

The Site Location is shown on Figure 1.1 of the EIA Report. The Site is situated within the Cloich Forest, covering an area of approximately 1,080 hectares (ha), centred on National Grid Reference (NGR) 320648, 647881 (Figure 1.2 of the EIA Report). The Site and the Development is wholly located within the administrative boundary of Scottish Borders Council ('the Council').

The topography of the Site, and immediate vicinity, is complex, with elevation ranging from approximately 280 metres (m) Above Ordnance Datum (AOD) in the north-east part of the Site to approximately 476 m AOD at the peak of Craillie Hill in the south. The Site encompasses the rolling Cloich Hills, including Peat Hill (466 m AOD), Ewe Hill (462 m AOD), White Rig (325 m AOD), and Craillie Hill (476 m AOD). The hills are dissected by a number of watercourses, including Middle Burn, Flemington Burn, Martyr's Dean, Corehope Burn and Harehope Burn. All watercourses eventually feed into the River Tweed. There are no waterbodies within the Site.

Coniferous plantation, at various stages of the planting, growing and felling cycle, is the primary land use within the Site; however, the area around Courhope in the south of the Site consists of improved upland pasture, utilised for sheep grazing, and improved grassland which remains clear of forestry.

In addition to the operational commercial forest of Cloich Forest, the Site and immediate vicinity consists of further areas of forestry and rural farmland, primarily used for grazing and other farmland activities.

The Site contains two public roads which form the Site access from the A703; these public roads are as follows:

- D17 Whim – Shiplaw; and
- D18 Cloich.

There are no residential properties within the Site; however, Cloich Farm is located adjacent to the Site, at approximate NGR 321655, 649105, approximately 1.2 km north-west from the closest turbine (T10).

### **2.2 Site Walkover**

The purpose of the desk study and site visit was to gain a thorough understanding of site conditions including topography, geology, existing peat instability and hydrology. The outcome of this stage of the study was to determine which areas required detailed intrusive survey (by peat probing) and ultimately provide data for the assessment of PSRA.

Several site visits were undertaken as part of the overall EIA process between March 2020 and March 2021 (these were supplemented with peat probing as detailed in Section 4). The Site was examined for evidence of peatlands, presence of landslip and localised haggling. Geological mapping and areas of interest were pre-loaded to a handheld device for reference during the site walkover. Following a review of these in parallel with the initial site walkover, the desk study aimed to identify and or verify the following:

- The general condition of peat deposits;
- Evidence of any previous peat instability;
- The presence of low lying wet/peat lands; and
- Watercourses and potential other receptors.



### **2.2.1 Site Conditions**

The current site conditions were informed in part by a review of aerial imagery sourced from Google Earth and Ordnance Survey (OS) online mapping. It can be seen that forestry plantations are present across a majority of the site at varying stages of development. Some southern and northern areas of the site have been subject to felling and currently comprise open hummocky ground. The images also show an established network of forestry tracks, which allow for relatively easy access throughout the Site, with exception to the north eastern area of the Site which does not facilitate vehicular access and consists of dense forestry which restricts access by foot. The aerial imagery was also used to identify areas at the Site where artificial drainage had occurred, the presence of existing access tracks, quarrying and forestry plantations, which all indicate the potential presence of artificial drainage which could have a dewatering effect on any surrounding peat. However, there is very little peat cover beneath the development footprint with only isolated pockets of deep peat noted in the surrounding areas, particularly the central and north-eastern site areas.

Topographically the Site is generally of high gradient, with extreme gradients falling in all directions from various hills in the south, east, west and central Site area.

Quarries are present in the eastern and western areas of the Site where rock has been extracted in specific areas. The presence of these quarries is known and they are not considered to pose any adverse impact to the Development.

Site photographs taken during the site walkover are included in Appendix B.

## **2.3 Published Geology**

### **2.3.1 Superficial Soils**

Published geological mapping of superficial soils indicates a majority of the Site to be underlain by deposits of Diamicton Till of Devensian Age. No superficial deposits are recorded across the remainder of the Site other than small localised pockets of Peat and Alluvium in the central eastern areas and at the northern extent of the Site.

Figure 9.1.2 illustrating the Superficial Soils is included in Appendix A.

### **2.3.2 Bedrock Geology**

Published bedrock geology mapping indicates the majority of the Site to be underlain by sandstone and siltstone of the Kirkcolm Formation, with wacke and siltstone of the Portpatrick Formation present in the south-western Site area. A thin lens of the Moffat Shale Group comprising mudstone is also present in the south-western Site area.

Figure 9.1.3 illustrating the Solid Geology is included in Appendix A.

### **2.3.3 Carbon and Peatland Mapping 2016**

The Carbon and Peatland 2016<sup>2</sup> Mapping indicates that at the macro level the Site is underlain by pockets of Class 4 soils in north, central and southern areas; these soils are unlikely to be associated with peatland habitats or to include carbon-rich soils. Numerous small pockets of Class 5 soils are also present at the Site, primarily in northern and central areas; these soils are not recorded as peatland habitat but there is potential for carbon-rich soils and deep peat. The remainder of the Site is recorded as Class 0 (Mineral Soils) where peatland habitats are not typically found, other than a small area of Class 3 soil which is recorded at the southern boundary of the Site; these are soils where occasional

---

<sup>2</sup> <https://www.nature.scot/professional-advice/planning-and-development/planning-and-development-advice/soils/carbon-and-peatland-2016-map> (Accessed 10/10/2022)

peatland habitats can be found and most soils are carbon-rich with some areas of deep peat.

## 2.4 Geomorphology

No evidence of historic peat haggling was noted during the Site walkover and topsoil, where undisturbed generally appeared to be in good condition. Extensive forestry plantation and quarrying activities have historically been undertaken at the Site; it is considered that properties of the peat deposits may have been altered due to these historical activities. Nonetheless, the possibility of instability within peat soils cannot be discounted, especially where there are significant topographic variances and the presence of watercourses, although there are only very localised areas of peat depth great enough to be considered at risk of instability.

## 2.5 Hydrology and Hydrogeology

The Site varies significantly in elevation and encompasses a network of watercourses which flow southwest and northeast from the central topographic high ridge.

The Site lies within the catchments of the Eddleston Water, which is classified by SEPA as having an overall status of "Poor", and Flemington Burn and Harehope Burn, which are both classified by SEPA as having an overall status of "Good"<sup>3</sup>.

The Cowieslinn Burn, a tributary of Eddleston Water, rises at the northwest boundary of the Site and flows northeast to join Eddleston Water approximately 1.3 km east of the Site. The Middle Burn rises in the centre of the Site, to the west of Peat Hill at approximately 430 m AOD and flows north to join the Cowieslinn Burn and Eddleston Water. The Eddleston Water discharges to the River Tweed in Peebles, approximately 6 km southeast of the Site.

The Early Burn rise to the east of the Site, flows northeast to form the Shiplaw Burn and eventually flows into the Eddleston Water and the River Tweed. There are a number of small tributaries associated with the Early Burn within the Site boundary.

The Courhope Burn rises in the centre of the Site to the northeast of Ewe Hill at approximately 450 m AOD and flows southwest to form the Flemington Burn at the western boundary of the Site. The Flemington Burn flows west and discharges to the Lyne Water and eventually the River Tweed approximately 5 km to the south of the Site.

There are a number of smaller tributaries of the Courhope Burn and Flemington Burn within the Site boundary, including Corbie Linn which is a tributary of Flemington Burn.

The Harehope Burn rises in the south of the Site, 100 m north of the southern boundary, and flows east to join the Eddleston Water and then joins the River Tweed at the confluence in Peebles.

A tributary of the Stewarton Burn is located to the southeast of the Site and drains to the east into Stewarton Burn and Wormiston Burn before discharging to the Eddleston Water approximately 2.5 km east of the Site.

The groundwater unit underlying the Development is the Peebles, Galashiels and Hawick groundwater unit which is classified by SEPA as having an overall status of "Good".

Figure 9.1.4 illustrating the Geomorphology of the Site is included in Appendix A

## 2.6 Sources of Information

The following sources of information were used as part of the desk study investigations:

---

<sup>3</sup> <https://www.sepa.org.uk/data-visualisation/water-environment-hub/> (Accessed 21/06/21)

- British Geological Survey - Online GeoIndex<sup>4</sup>;
- Ordnance Survey (OS) topographical information;
- Aerial and Satellite photography via Ordnance Survey and Google Earth.
- Soil Survey of Scotland - 'MacAulay Institute for Soil Research' 1984;
- Soil Survey of Scotland - 'Scottish Peat Surveys' 1964;
- Scottish Government (SG) - 'Peat Landslide Hazard and Risk Assessments' December 2017;
- Scottish Government, Scottish Natural Heritage, SEPA (2017) Peatland Survey, Guidance on Developments on Peatland<sup>5</sup>;
- The Scottish Government - Scotland's Third National Planning Framework, 2014<sup>6</sup>;
- The Scottish Government - Scottish Planning Policy, 2014<sup>7</sup>;
- Assessments by other EIA specialists (specifically hydrology and ecology for data on sensitive receptors); and
- Scotland's Environment Interactive Map<sup>8</sup>

---

<sup>4</sup> <https://mapapps2.bgs.ac.uk/geoindex/home.html> (Accessed 10/10/22)

<sup>5</sup> <https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2018/12/peatland-survey-guidance/documents/peatland-survey-guidance-2017/peatland-survey-guidance-2017/govscot%3Adocument/Guidance%2Bon%2Bdevelopments%2Bon%2Bpeatland%2B-%2Bpeatland%2Bsurvey%2B-%2B2017.pdf> (Accessed 21/06/21)

<sup>6</sup> <https://www.gov.scot/publications/national-planning-framework-3/> (Accessed 21/10/22)

<sup>7</sup> <https://www.gov.scot/publications/scottish-planning-policy/> (Accessed 21/10/22)

<sup>8</sup> <https://map.environment.gov.scot/sewebmap/> (Accessed 21/10/22)

### **3 GUIDANCE AND METHODOLOGY**

#### **3.1 Overview of Guidance and Peat Failure Mechanisms**

##### **3.1.1 Peat Depth and Slope**

The Scottish Government guidance (as referenced above) divides peat instability into two categories: 'peat slides' and 'bog bursts'. The guidance states that peat slides have a greater risk of occurrence in areas where:

- Peat is encountered at or near to ground surface level;
- The thicknesses are recorded in the region of 2.0 m (above which, in general terms, peat instability would increase with peat thickness); and
- The slope gradients are steep (between 5° and 15°).

Bog bursts are considered to have a greater risk of occurrence in areas where:

- Peat depth is greater than 1.5 m; and
- Slope gradients are shallow (between 2° and 10°).

It should be noted however that peat instability events, although uncommon, can occur out with these limits. Reports of bog bursts are generally restricted to the Republic and Northern Ireland.

Further to the general guidance above, in relation to peat depth, it is considered that the extent and depth of peat is controlled to a degree by rainfall and elevation, giving rise to three common types of peat (Boylan et al. 2008<sup>9</sup>):

- Upland Blanket Bog: Blanket bogs are typically about 3 m thick however, they can be up to 5 m thick. Generally thinning at greater elevations;
- Raised Bog: Raised bogs generally tend to be 3-12 m thick, averaging 7 m with their growth occurring above the water table; and
- Lowland Blanket Bog: Much the same as the upland version; however, they form around sea level in areas of very high rainfall.

Generally, the potential for peat instability increases with peat depth, however other instability indicators need considered, namely slope and substrate.

##### **3.1.2 Substrate**

Peat slide failures tend to occur at the interface of the peat and underlying substrate therefore, understanding the nature of the underlying substrate can provide a key factor when considering the risk stability.

Using the peat probe refusal, an estimation of the underlying materials can be determined based on:

- Gradual refusal – Clay;
- Crunching/Gritty – Weathered Rock/Sand and Gravel; or
- Abrupt Refusal/Hard – Rock.

Where sand and/or gravel is recorded, the interface is considered to be the best-case scenario with the highest friction value.

Where clay is recorded, the upper horizons of the clay are typically softened through poor drainage in this soil group with low shear strengths expected. While rock substrate provides a high strength, the surface being smooth can lead to a weak interface, with similar risk to that of a clay substrate.

---

<sup>9</sup> Boylan et al (2008) Peat Slope Failure in Ireland (Accessed 10/10/22)

The presence of slip material, or evidence of peat instability would represent the worst-case scenario for the assessment of substrate.

The substrate parameters are included in the Hazard and Exposure Assessment in Section 5 of this PSRA.

### 3.1.3 Other Considerations

Preparatory factors which effect the stability of peat slopes in the short to medium-term include:

- Loss of surface vegetation (deforestation);
- Changes in sub-surface hydrology;
- Increase in the mass of peat through accumulation, increase in water content and growth of tree planting; or
- Reduction in shear strength of peat or substrate due to chemical or physical weathering, progressive creep and tension cracking.

Triggering factors which can have immediate effect on peat stability and act on susceptible slopes include:

- Intensive rainfall or snow melt causing pressures along existing or potential peat/substrate interfaces;
- Snow melt;
- Alterations to drainage patterns, both surface and sub-surface;
- Peat extraction at the toe of the slope reducing the support of the upslope material;
- Peat loading (commonly due to stockpiling) causing an increase in shear stress; and
- Earthquakes or rapid ground accelerations such as due to blasting or mechanical movement.

Consideration of peat stability should form an integral part of the design of a wind farm development. While peat does not wholly provide a development constraint, areas of deep peat or peat deposits on steep slope should be either avoided through design and micro-siting; or mitigation measures should be designed to avoid instability and movement.

## 3.2 Methodology

Despite being an application under the Town and Country Planning (Scotland) Act 1997<sup>10</sup>, the PSRA has been carried out in accordance with the Energy Consents Unit (ECU), Scottish Government guidance of 2017 titled Peat Landslide Hazard and Risk Assessments - Best Practice Guide for Proposed Electricity Generation Developments<sup>11</sup>.

In June 2014, Scottish Planning Policy<sup>12</sup> (SPP) and National Planning Framework (NPF3)<sup>13</sup> were published. In relation to peat and the assessment of effects on resource, NPF3 references SNH Scotland's National Peatland Plan<sup>14</sup>. These policy, framework and guidance documents are considered in this PSRA. The PSRA undertaken is based on:

- Desk based assessment;
- Site Walkover;
- An initial Phase 1 peat probing scheme;

---

<sup>10</sup> Scottish Government (1997) Town and Country Planning (Scotland) Act 1997 [Online] Available at: <http://www.legislation.gov.uk/ukpga/1997/8/contents> (Accessed 21/06/21)

<sup>11</sup> Scottish Government (2017) Peat Landslide Hazard and Risk Assessment: Best Practice Guide for Proposed Electricity Generation Development [Online] Available at: <https://www.gov.scot/Publications/2017/04/8868> (Accessed 21/06/21)

<sup>12</sup> Scottish Government (2014) Scottish Planning Policy [Online] Available at: <http://www.scotland.gov.uk/Topics/Built-Environment/planning/Policy> (Accessed 21/06/21)

<sup>13</sup> Scottish Government (2014) National Planning Framework 3 [Online] Available at: <http://scotland.gov.uk/Resource/0045/00453683.pdf> (Accessed 21/06/21)

<sup>14</sup> SNH (2015) Scotland's National Peatland Plan [Online] Available at: <https://www.nature.scot/climate-change/taking-action/carbon-management/restoring-scotlands-peatlands/scotlands-national-peatland-plan> (Accessed 21/06/21)

- Phase 2 probing comprising infrastructure specific probing; and
- A hazard and risk ranking assessment.

The area of the Site subject to assessment was determined by the emerging development layout which considered both anticipated peat deposits as well as other physical and environmental constraints.

### ***3.2.1 Development of Hazard Rank***

The early stages of the PSRA including the desk study, site visit and peat probing were carried out in parallel with the assessment of wider constraints to inform the layout of the Development. These assessments were once again carried out during the SEI following the relocation of T8 and addition of the new TCC. Following identification of peat depths within the Site, the assessment has determined the potential effects on the peat resource from construction activities which would include:

- Construction of tracks;
- Excavation of turbine bases;
- Foundation construction;
- Construction of hardstanding; and
- Temporary storage of peat and soils.

An assessment of the peat probing data and a review against desk study information was undertaken and a hazard rank was calculated for different zones across the site reflecting risk of peat instability/constraint to construction.

The EIA Report Layout achieved a 'negligible or low' hazard ranking, with half of the hazard zones ranked as 'low.' Where practical, the SEI Layout would be progressed to avoid areas of a risk score above 'low'. Where this has would not be achievable, areas affected would be discussed in the SEI as having significant effect, with relative mitigation measures proposed to reduce this, and recorded on a risk register which sets out specific mitigation measures which are considered necessary to reduce the risk of inducing instability.

Details of the hazard and risk ranking assessment is included in Sections 5 and 6 of this PSRA.

## **4 SITE SURVEYS AND RESULTS**

### **4.1 Investigations**

The existing peat depths across the Site have been determined through peat probe surveys undertaken during both the EIA and SEI as recommended in the NatureScot (formerly Scottish Natural Heritage (SNH)), Scottish Government and James Hutton Institute guidance for investigating peat. The initial surveys were initiated to inform the EIA and site design work while supporting the peat slide risk assessment and comprised of the following:

- Phase 1 Probing – 100 m grid across the developable area; and
- Phase 2 (a and b) Probing – Infrastructure focussed probing comprising 50 m centres along tracks with perpendicular probes between 10 m and 25 m either side of track, and 10 m cross-hair of turbine locations.

Initial peat depth surveys were undertaken in March 2020 comprising a 100 m grid in the developable area and where dense forestry plantation would allow access. The rationale of probing is in accordance with the phase 1 approach as detailed in the Scottish Government guidance for investigating peat.

Phase 2 peat depth surveys were undertaken across a series of visits in November 2020 through to April 2021. The probe positions for these visits were determined by the design freeze for the EIA Report Layout and provided increased resolution along the access track alignments and in the vicinity of turbine hardstandings. Peat depths were measured at cross sections centred along the proposed access tracks at 50 m centres with offsets of 25 m on either side of the centre line. Across turbine locations, where possible, probing was carried out at 10 m centres for assessment allowing for micro siting of turbines and hardstandings relative to prevailing conditions.

The peat probe surveys carried out as part of the SEI specifically targeted the revised and newly proposed infrastructure. At the revised T8 location, probes were sunk at 10 m centres across the turbine location, while the crane hardstanding and access track were probed according to the Site layout. At the additional TCC, the proposed infrastructure area was probed in a 25 m x 25 m grid formation.

It should be acknowledged that natural variations in peat depth/thickness could occur between probe positions, although areas of infrastructure had undergone intensely spaced probing and this would be less likely.

### **4.2 Summary of Peat Depths**

Throughout the peat surveys to date, a total of 1,129 probes were progressed, 1,082 during the initial EIA surveys and 47 probes during the SEI. 92.4% of these probes recorded no peat or peat up to 0.5 m in depth. Thick peat (where the depth was greater than >1.0 m) was recorded at less than 3% of locations.

The maximum peat depth recorded was 4.6 m in the eastern sector of the Site, this was the only peat of this extent found in the entire Site.

Generally, peat over the Site was recorded as being less than 0.5 m with the average peat depth across the Site being 0.26 m.

Table 4.1 summarises the recorded peat depths.

**Table 4.1: Peat Depth Summary**

Peat Depth Range (m)	No. of peat probes	Percentage of Total (%)
0.00 - 0.50 m	1,043	92.4
0.51m - 1.00 m	55	4.9
1.01m - 1.50 m	12	1.1
1.51m - 2.00 m	8	<1.0
2.01m - 2.50 m	3	<1.0
2.51m - 3.00 m	0	0
3.01m - 3.50 m	4	<1.0
3.51m - 4.00 m	0	0
4.01m - 4.50 m	3	<1.0
4.51m - 5.00m	1	<1.0

The peat probe locations and depths are shown on Figure 9.1.5 appended with this PSRA, and details of probe records are included in Appendix C. The Interpolated Peat Depths are illustrated on Figure 9.1.6 (determined using the Inverse Distance Weighting (IDW) method of interpolation) and the peat depths encountered at turbine locations and summarised in Table 4.2 below.

**Table 4.2: Peat Depths at Turbines**

Proposed Turbine No.	Average Peat Depths (m)
T1	0.16
T2	0.18
T3	0.28
T4	0.13
T5	0.21
T6	0.16
T7	0.06
T8	0.07
T9	0.12
T10	0.13
T11	0.10
T12	0.11



## 5 HAZARD AND EXPOSURE ASSESSMENT

### 5.1 Background

A 'Hazard Ranking' system has been applied across the Site based on the analysis of risk of peat slide as outlined in the Scottish Government guidance. This is applied on the principle:

$$\text{Hazard Ranking} = \text{Hazard} \times \text{Exposure}$$

Where 'Hazard' represents the likelihood of any peat slide event occurring and 'Exposure' being the impact or consequences that a peat slide may have on sensitive receptors that exist on and around the Site.

### 5.2 Methodology

The determination of Hazard and Exposure values is based on a number of variables which impact the likelihood of a peat slide (the Hazard), and the relative importance of these variables specific to the Site.

Similarly, the consequences or Exposure to receptors is dependent on variables including the particular scale of a peat slide, the distance it will travel and the sensitivity of the receptor.

In the absence of a predefined system, the approach to determining and categorising Hazard and Exposure is determined on a Site-by-Site basis. The particular system adopted for the Development PSRA assessment is outlined in the following sub sections.

### 5.3 Hazard Assessment

The potential for a peat slide to occur during the construction of a windfarm depends on several factors, the importance of which can vary from Site to Site. The factors requiring considerations would typically include:

- Peat depth;
- Slope gradient;
- Substrate material;
- Evidence of instability or potential instability;
- Vegetation cover; and
- Hydrology.

Of these, peat depth and slope gradient are considered to be principal factors. Without a sufficient peat depth and a prevailing slope, peat slide hazard would be negligible. The Slope Gradient is illustrated on Figure 9.1.7 for the Development (see Appendix A), the substrate material is also considered a key relevant factor in relation to the mechanics of slide, whilst the other aspects provide key considerations. The slope data is derived from Ordnance Survey 5m Digital Terrain Model (OS 5m DTM). It should be noted that historical peat probing at the Site did not include an estimate of the underlying substrate material, therefore a value of 2 (unknown) was assigned to these probing points which is equivalent to clay as seen in Table 5.1. This is considered a conservative figure which could increase the hazard ranking and is another layer of safety embedded within this PSRA.

The other factors have not been assigned coefficients but have nonetheless been built into the assessment. In regards to hydrology, major and minor watercourses are assigned different coefficients to reflect the sensitivity of the receptor with the distance of each probe from a watercourse affecting its hazard ranking.

No existing peat instability risks have been recorded at the Site. However, should slip material be recorded at a probing point, this will be incorporated into the hazard assessment and is assumed to be the highest potential level of hazard. Therefore, the highest substrate coefficient will be applied.

Vegetation plays a key role on both peatland quality and in reducing the risk of instability in peatland. It gives structure to the upper soil horizons and acts as an important regulator of water content in peat above the water table. The presence of bare or eroded peat can indicate an instability risk due to the lack of supporting vegetation. No bare or eroded peat has been recorded at the Site, but there is a substantial forestry area on Site, some of which needs to be felled prior to the construction phase. This presents a risk of instability due to the removal of long-established roots and resulting lack of vegetation. Due to the shallow peat in the areas where felling will be required, it is deemed that the removal of vegetation will not result in an increased peat slide risk. Further details of vegetation present at the Site are discussed in **Chapter 7: Ecology** of the EIA Report and its associated Technical Appendices.

## 5.4 Hazard Rating

When several factors may impact on the Hazard potential, a relative ranking process is applied attributing different weighting to each factor as shown below.

**Table 5.1: Coefficients for Slope Gradients**

Slope Angle (degrees)	Slope Angle Coefficients
Slope < 2°	1
2° < Slope < 4°	2
4° < Slope < 8°	4
8° < Slope < 15°	6
Slope >15°	8

**Table 5.2: Coefficients for Peat Thickness and ground conditions**

Peat Thickness	Ground Conditions Coefficients
Peaty or organic soil (<0.5m)	1
Thin Peat (0.5 – 1.0m)	2
Deep Peat (>1.0m)	3*
Deep Peat (>3.0)	8

\* - Note that thicker peat generally occurs in areas of shallow gradient and records and research indicate that thick peat does not generally occur on the steeper gradients.

**Table 5.3: Coefficients for Substrate**

Substrate Material	Substrate Coefficients
Sand/gravel	1
Rock	1.5
Clay	2
Not proven	2
Slip material (Existing materials)	5

The Hazard Rating Coefficient for a particular location is calculated using the following equation:

$$\text{Hazard Rating Coefficient} = \text{Slope Gradient} \times \text{Peat Thickness} \times \text{Substrate}$$

From the Hazard Rating Coefficient, the risk to stability can be ranked as set out in Table 5.4.

**Table 5.4: Hazard Rating**

Hazard Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<5	Negligible
5 to 15	Low
16 to 30	Medium
31 to 50	High
> 50	Very High

## 5.5 Peat Stability Assessment

The likelihood of a particular slope or hillside failing can be expressed as a Factor of Safety. For any potential failure surface, there is a balance between the weight of the potential landslide (driving force or shear force) and the inherent strength of the soil or rock within the hillside (shear resistance).

The guidance states that the 'Infinite Slope' method of analysis, after Skempton and DeLory (1957), is the most well established and commonly applied method for the assessment of peat slope stability. The stability of a slope can be assessed by calculating the factor of safety  $F$ , which is the ratio of the sum of resisting forces (shear strength) and the sum of the destabilising forces (shear stress):

$$F = \frac{c' + (\gamma - m\gamma_w)z \cos^2 \beta \tan \phi'}{\gamma z \sin \beta \cos \beta}$$

Where  $c'$  is the effective cohesion,  $\gamma$  is the bulk unit weight of saturated peat,  $\gamma_w$  is the unit weight of water,  $m$  is the height of the water table as a fraction of the peat depth,  $z$  is the peat depth in the direction of normal stress,  $\beta$  is the angle of the slope to the horizontal and  $\phi'$  is the effective angle of internal friction. Values of  $F < 1$  indicate a slope would have undergone failure under the conditions modelled; values of  $F > 1$  suggest conditions of stability.

In the absence of any historical hydrological monitoring, an assumption on groundwater levels has been adopted for the assessment, that 90% of the peat column at each probe location is below the water table, an overall conservative approach. While the assessment considers the recorded data at each of the peat probes to establish hazard ranking for the purposes of the peat stability analysis, groundwater depth is conservatively assumed to be within close proximity of the surface, based on the understanding of peat and its hydrological properties that it can consist of up to 90% water by volume.

Assumed geotechnical parameters have been utilised in the formula to inform the stability assessment, based on literature values to inform the stability analysis, as included in Table 5.5.

**Table 5.5: Literature for Geotechnical Parameters of Peat**

Reference	Effective Cohesion C' (kPa)	Effective Angle of Friction $\phi$ (°)	Unit Weight Y (kN/m <sup>2</sup> )	Comments
Hanrahan et al (1967) <sup>15</sup>	5.5 – 6.1	36.6 - 43.5	-	Remoulded H4 Sphagnum peat
Hollingshead and Raymond (1972) <sup>16</sup>	4.0	34	-	-
Hollingshead and Raymond (1972)	2.4 – 4.7	27.1 – 35.4	-	Sphagnum peat (H3, mainly fibrous)
Carling (1986) <sup>17</sup>	6.52	0	10	-
Kirk (2001) <sup>18</sup>	2.7 – 8.2	26.1 – 30.4		Ombrotrophic blanket peat
Warburton et al (2003) <sup>19</sup>	5.0	23	9.68	Basal Peat
Warburton et al (2003)	8.74	21.6	9.68	Fibrous Peat
Dykes and Kirk (2006)	3.2	30.4	9.61	Acrotelm
Dykes and Kirk (2006)	4.0	28.8	9.71	Catotelm

C' – effective cohesion (kPa), typically ranging from 2.5 to 8.5 therefore 5.0 has been adopted for the purposes of the assessment.

$\phi$  – effective angle of friction (°), typically ranging from 21.6 to 43.5 therefore 29.6 has been adopted for the purposes of the assessment.

Y – unit weight (kN/m<sup>2</sup>), typically ranging from 9.61 to 10, therefore 10 has been adopted for the purposes of the assessment.

In accordance with the best practice method, F values of <1.0 indicate slopes that would experience failure under the modelled conditions and as such are considered areas of high risk. However, Boylan et al (2008) indicate that a relatively high value of F=1.4 should be used to identify slopes with the potential for instability. Adopting this approach, high risk areas are indicated where F is <1.0, medium risk areas are indicated as 1.01 to 1.50 and >1.5 are low risk.

Using digital terrain modelling and GPS co-ordinates of each peat probe, a factor of Safety, F has been calculated for each probe locations which has been interpolated through ArcGIS Spatial Analyst tools. The Factor of Safety Assessment provides a sense check of the ranking based system, providing an absolute approach to the 'Factor of Safety Plan' is shown on Figure 9.1.8 (see Appendix A). The results of the Factor of Safety calculations

<sup>15</sup> Hanrahan et al (1967) - Hanrahan, E.T., Dunne, J.M., and Sodha, V.G. 1967. Shear strength of peat. Proceedings Geotechnical Conference, Oslo, Vol. 1, pp. 193–198.

<sup>16</sup> Hollingshead and Raymond (1972) - Hollingshead, G.W., and Raymond, G.P. 1972. Field loading tests on Muskeg, Canadian Geotechnical Journal, 9(3): 278–289.

<sup>17</sup> Carling (1986) - Peat slides in Teesdale and Weardale, northern Pennines, July 1983: Description and failure mechanisms

<sup>18</sup> Kirk (2001) - Initiation of a multiple peat slide on Cuilcagh Mountain, Northern Ireland

<sup>19</sup> Warburton et al (2003) - Anatomy of a Pennine peat slide, Northern England

indicated all points on the Site as low risk. This was primarily due to the limited peat recorded on the Site.

## 5.6 Exposure Assessment

The main Exposure receptors identified within the Site and surrounding area which could potentially be affected in the event of a peat slide were existing wind farm infrastructure.

The impact of a peat slide on receptors can be assessed on a relative scale based on the potential for loss of habitat, a historical feature or disruption/danger to the public. To effectively assess the impact, the assessment of Exposure effect must also consider the distance between the hazard and the receptor, and the relative elevation between the two.

## 5.7 Exposure Rating

Similar to the Hazard Rating, the Exposure Ratings were determined using relative ranking process by attributing the different weighting systems to each factor as shown below:

**Table 5.6: Coefficients for Receptor Type**

Receptor	Receptor Coefficients
Tracks or Paths	2
Road	3
Minor water feature	6
Site infrastructure	6
Dwelling	8
Major water feature	8
Sensitive Habitats (Blanket bog)	8

**Table 5.7: Coefficients for Distance from Receptor**

Distance from Receptor	Distance Coefficients
> 1 km	1
100 m to 1 km	2
10 m to 100 m	3
<10 m	4

**Table 5.8: Coefficients for Receptor Elevation**

Receptor Elevation	Elevation Coefficients
< 10 m	1
10 m to 50 m	2
50 m to 100 m	3
> 100 m	4

The Exposure Rating Coefficient for a particular location is calculated using the following equation:

$$\text{Exposure Rating Coefficient} = \text{Receptor} \times \text{Distance} \times \text{Elevation}$$

From the Exposure Rating Coefficient, the risk to stability can be ranked as set out in Table 5.9.

**Table 5.9: Exposure Rating**

Exposure Rating Co-efficient	Potential Stability Risk (Pre-Mitigation)
<6	Very Low
6 to12	Low
13 to 24	High
24 to 30	Very High
>30	Extremely High

## 5.8 Rating Normalisation

In order to achieve an overall Hazard Ranking in accordance with the Scottish Government Guidance, the Hazard and Exposure Rating Coefficient derived from the coefficient tables are normalised as shown in Table 5.10.

**Table 5.10: Rating Normalisation**

Hazard Rating		Exposure Rating	
Current Scale	Normalised Scale	Current Scale	Normalised Scale
<5 Negligible	1	<6 Very Low	1
5 to 15 Low	2	6 to 12 Low	2
15 to 30 Medium	3	13 to 24 High	3
30 to 50 High	4	25 to 30 Very High	4
>50 Very high	5	>30 Extremely High	5

The record of the Hazard Rank Assessment is included in Appendix C of this PSRA.

## 6 HAZARD RANKING

Having identified the rating coefficients in Section 5 of this PSRA, it is possible to categorise areas of the Site with a Hazard Ranking by multiplying the Hazard and Exposure Rating. Hazard Ranking and associated suggested actions matrix are shown in Tables 6.1 and 6.2 below:

**Table 6.1: Hazard Ranking and Suggested Actions**

Hazard Ranking		Action Suggested in the Scottish Government Guidance (as referenced above)
17-25	High	Avoid project development at these locations.
11-16	Medium	Project should not proceed unless hazard can be avoided or mitigated at these locations, without significant environmental impact, in order to reduce hazard ranking to low or less
5-10	Low	Project may proceed pending further investigation to refine assessment. Mitigation of hazards maybe required through micro-siting or re-design at these locations.
1-4	Negligible	Project should proceed with monitoring and mitigation of peat landslide hazards at these locations as appropriate.

**Table 6.2: Hazard Ranking Matrix**

<b>Hazard Rating</b>	5	Low	Low	Medium	High	High
	4	Negligible	Low	Medium	Medium	High
	3	Negligible	Low	Low	Medium	Medium
	2	Negligible	Negligible	Low	Low	Low
	1	Negligible	Negligible	Negligible	Negligible	Low
		1	2	3	4	5
		<b>Exposure Rating</b>				

Receptor exposure was assessed for each of the hazard zones using the approach in Section 5. A summary of the Hazard Ranking result for each identified area is summarised in Table 7.1 and is presented in Figure 9.1.9 - Hazard Ranking Zonation Plan (see Appendix A). The zonation is based on a combination of considerations including calculated hazard result, peat depth, topography and receptors and land uses.

## **7 SLIDE RISK AND MITIGATION**

### **7.1 General**

The PSRA has shown the Site to be of 'negligible' or 'low' hazard ranking.

The majority of peat across the site area was less than 0.5 m, with some also extending to depths between 0.5 m and 1.0 m. Localised pockets of peat greater than 1.0 m were recorded and these areas were largely avoided through the design development process.

The previous location of T8 was in an area with average peat depth of 0.48m and a 'negligible' hazard ranking. The new location of T8 is within an area of shallower peat with an average depth of 0.07m and remains in an area of 'negligible' hazard ranking.

As part of the SEI an additional TCC has been added for Scottish Power Transmission within the northern area of the Site. The additional TCC is located in an area with average peat depths of 0.42m and was assessed to pose a 'negligible' hazard ranking in relation to peat slide. Following the completion of the SEI process, the additional TCC remains in a 'negligible' hazard rank area.

Where the hazard ranking has been lowered through mitigation measures set out in Section 7.2 and 7.3 of this PSRA, the original ranking will remain in the overall hazard zoning plan. It should be acknowledged that the hazard zonation plan is based on the pre-mitigation status.

While specific recommended mitigation in 'low' ranked areas are proposed, other mitigation is embedded in the design at EIA stage. It is also necessary for detailed design and construction of the Development to be undertaken in a competent and controlled manner.

The embedded mitigation and good practice measures are set out in Section 7.2 of this PSRA. It should be noted that the mitigation measures defined are not exclusive and other forms of mitigation may be required, as a result of conclusions from ground investigations undertaken prior to detailed design for example, and should be implemented during construction of the Development.



**Table 7.1: Hazard Ranking**

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
Hazard Area	Infrastructure Affected	Ranking	Key Aspects and Direct Effects	Specific Actions	Ranking
<b>H1</b>	Existing tracks, Substation, BESS, and both Temporary Construction Compounds	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Northern portion of site, sloping northerly</li> <li>Hydrology: Middle burn situated in the central area flowing north.</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 8°</li> <li>Exposure: Proposed infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H2</b>	Proposed track, T12 and Borrow Pit	Low	<ul style="list-style-type: none"> <li>Location and topography: sloping slightly to the north and more steeply to the south with the plateau West Side Hill in in the central area.</li> <li>Hydrology: Tributaries from surrounding hills, flowing north.</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 18°</li> <li>Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>During construction, visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H3</b>	T10	Low	<ul style="list-style-type: none"> <li>Location and topography: South side of Peat</li> <li>Hydrology: Middle Burn and tributary to Early Burn</li> <li>Peat Depth: 0.0 m – 2.50 m.</li> <li>Generally &lt; 0.50m</li> <li>Slope Gradient: 0° to &lt;20°</li> <li>Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>During construction, visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H4</b>	n/a	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Slightly sloping topography in the valley between West Side and Peat Hill.</li> <li>Hydrology: None noted</li> <li>Peat Depth: 0.0 m – 1.50 m. Generally, &lt; 0.50 m</li> <li>Slope Gradient: 0° to 14°</li> <li>Exposure: None</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H5</b>	T10 and Proposed Tracks	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Sloping topography on south-eastern face of Peat Hill.</li> <li>Hydrology: None noted</li> <li>Peat depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 4° to 16°</li> <li>Exposure: Proposed Site Infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
				Mitigation measures as set out in section 7.3.	
<b>H6</b>	Proposed track, existing track	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Generally flatter topography, within the north eastern area of main body of site.</li> <li>Hydrology: Tributaries to the Early Burn</li> <li>Peat Depth: 0.0 m - 4.50 m. Varying depths of peat with isolated are of deep peat located in the shallowest topographic area.</li> <li>Slope Gradient: 0° to 30°</li> <li>Generally 0 - 8°</li> <li>Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H7</b>	n/a	Low	<ul style="list-style-type: none"> <li>Location and topography: Generally flatter topography, within the north eastern area of main body of site.</li> <li>Hydrology: Tributaries to the Early Burn</li> <li>Peat Depth: 0.0 m - 3.50 m. Varying depths of peat with isolated are of deep peat located in the shallowest topographic area.</li> <li>Slope Gradient: 0° to 8°</li> <li>Exposure: None</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>During construction, visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
H8	Proposed track, existing track and T11	Low	<ul style="list-style-type: none"> <li>Location and topography: Steep valley in the western site area within Cloich Hills</li> <li>Hydrology: Flemington Burn and tributaries</li> <li>Peat Depth: 0.0 m - 1.50 m. Generally, &lt;0.50 m</li> <li>Slope Gradient: 0° to 16°</li> <li>Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>During construction, visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
H9	T6	Low	<ul style="list-style-type: none"> <li>Location and topography: Sloping area in the west of site, on face of Ewe Hill.</li> <li>Hydrology: Tributary to Flemington Burn</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 2° to 18°</li> <li>Exposure: Site infrastructure and Borrow pit area</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>During construction visual inspections and monitoring in areas with the potential for peat slide risk should take place.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H10</b>	Proposed track, T1 and T8	Negligible	<ul style="list-style-type: none"> <li>• Location and topography: Plateau along top of Ewe Hill and Whaup Law in the Central site area.</li> <li>• Hydrology: Gibbs Cloich</li> <li>• Peat Depth: 0.0 m – 2.00 m. Generally, &lt;0.50 m</li> <li>• Slope Gradient: 0° to 20°</li> <li>• Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H11</b>	Proposed track, T7 and T9	Negligible	<ul style="list-style-type: none"> <li>• Location and topography: Steep southern face of Ewe Hill in the central site area.</li> <li>• Hydrology: Muirhope Glen, and tributary to the Courhope Burn</li> <li>• Peat Depth: 0.0 m - 0.50 m.</li> <li>• Slope Gradient: 4° to &lt;22°</li> <li>• Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outline in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H12</b>	Proposed Tracks and Borrow Pit	Low	<ul style="list-style-type: none"> <li>• Location and topography: Valley between Ewe Hill/Whaup Law and the southern face of Kilrubie Hill.</li> <li>• Hydrology: Martyr's Dean and Tributaries to the Courhope Burn</li> <li>• Peat Depth: 0.0 m – 1.50 m. Generally, &lt;0.50 m</li> <li>• Slope Gradient: 0° to &lt;18°</li> <li>• Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outline in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H13</b>	T5	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Eastern Site Area, slightly sloping topography.</li> <li>Hydrology: None</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 16°</li> <li>Exposure: Site infrastructure</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H14</b>	T4 and Proposed Tracks	Low	<ul style="list-style-type: none"> <li>Location and topography: Sloping topography on the eastern face of Kilrubie Hill, in the eastern site area.</li> <li>Hydrology: None</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 16°</li> <li>Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H15</b>	Proposed Tracks	Low	<ul style="list-style-type: none"> <li>Location and topography: Sloping topography on the southern and western face of Ewe Hill.</li> <li>Hydrology: Gibbs Cloich, Muirhope Glen and Courhope Burn</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 18°</li> <li>Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H16</b>	None	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Gently sloping topography between Ewe Hill and Crailzie Hill.</li> <li>Hydrology: Courhope Burn</li> <li>Peat Depth: 0.0 m – 0.50 m.</li> <li>Slope Gradient: 0° to 16°</li> <li>Exposure: Hydrology</li> </ul>	<p>Construction Environmental Management Plan and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>No infrastructure or construction activity is proposed in this area at the south western extent of the Site. Nonetheless, visual inspections and monitoring in the area should take place during the construction phase.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible



Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H17</b>	Proposed Tracks, T2 and T3	Low	<ul style="list-style-type: none"> <li>Location and topography: Southern site area between Craillie Hill and Ewe Hill.</li> <li>Hydrology: Muirhope Glen</li> <li>Peat Depth: 0.0 m – 1.00 m. Generally &lt;0.5m</li> <li>Slope Gradient: 0° to 14°</li> <li>Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible
<b>H18</b>	Proposed Tracks	Negligible	<ul style="list-style-type: none"> <li>Location and topography: Southern site area between Craillie Hill and Ewe Hill.</li> <li>Hydrology: Tributary to Courhope Burn</li> <li>Peat Depth: 0.0 m – 0.5 m.</li> <li>Slope Gradient: 2° to 14°</li> <li>Exposure: Site infrastructure, Hydrology</li> </ul>	<p>Best practice measures in relation to drainage prior to and during construction will be implemented as outlined in Technical Appendix A10.1 Water Construction Environmental Management Plan of the EIA Report and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

Hazard Area and Infrastructure		Unmitigated Hazard		Mitigated Hazard	
<b>H19</b>	None	Negligible	<ul style="list-style-type: none"> <li>• Location and topography: Eastern Site area between Kilrubie Hill and Craizie Hill.</li> <li>• Hydrology: Tributary to Stewarton Burn</li> <li>• Peat Depth: 0.0 m – 0.5 m.</li> <li>• Slope Gradient: 0° to 14°</li> <li>• Exposure: Hydrology</li> </ul>	<p>Construction Environmental Management Plan and management of peat and peaty soils as outlined in Technical Appendix A9.2 Outline Peat Management Plan of the SEI Report.</p> <p>No infrastructure or construction activity is proposed in this area at the south eastern extent of the Site. Nonetheless, visual inspections and monitoring in the area should take place during the construction phase.</p> <p>Mitigation measures as set out in section 7.3.</p>	Negligible

## 7.2 Embedded Mitigation

Embedded mitigation includes measures taken during design of the SEI Layout to reduce the potential for peat slide risk, designing to avoid any localised deep pockets of peat as well as consideration of wider environmental constraints, including the hydrology on Site. In summary the principal measures that have been taken in relation to avoiding peat slide are:

- Locating infrastructure on shallower slopes, where possible; and
- Locating infrastructure on areas of shallow peat (or no peat) where possible.

Section 7.3 will detail the types of mitigation that will be employed prior to and during construction to reduce potential risk.

## 7.3 Peat Slide Mitigation Recommendations

Mitigation measures and good practice procedures will be implemented during construction including:

- Ground investigations prior to detailed design;
- Identification of areas sensitive to changes in drainage regime prior to detailed design;
- Implementation of a geotechnical risk register where the contractor will be responsible for appointing a chartered geotechnical engineer who will monitor any potential stability risks for periodic monitoring programme through construction;
- Identification of areas of deep peat and tool box talks on limiting the works in these areas. There is no significant peat present beneath the footprint of the Development;
- Micro siting turbines and other infrastructure where required;
- Management of peat, soils and rock where necessary to predetermined temporary storage areas, and managed by the onsite ECoW when required;
- Avoid placing excavated material or other forms of loading on breaks of slope or other potentially unstable slopes;
- Excavation works should not be during periods of continuous heavy rainfall after heavy and prolonged rainfall events; and
- Post-construction reinstatement and re-establishment of vegetation at earliest;
- Appropriate drainage design should be implemented trackside and at turbines and crane hardstands.

## **8 CONCLUSIONS**

This PSRA has been undertaken for the Development in accordance with best practice, as detailed in Section 4.2 of the PSRA. The early stages of the assessment included a desk study, review of historic peat probing across the Site, followed by completion of Phase 1 peat probing and a further intensive probing exercise on the design of the SEI Layout. The information gathered during this investigation was used to develop a Hazard Ranking across the Site.

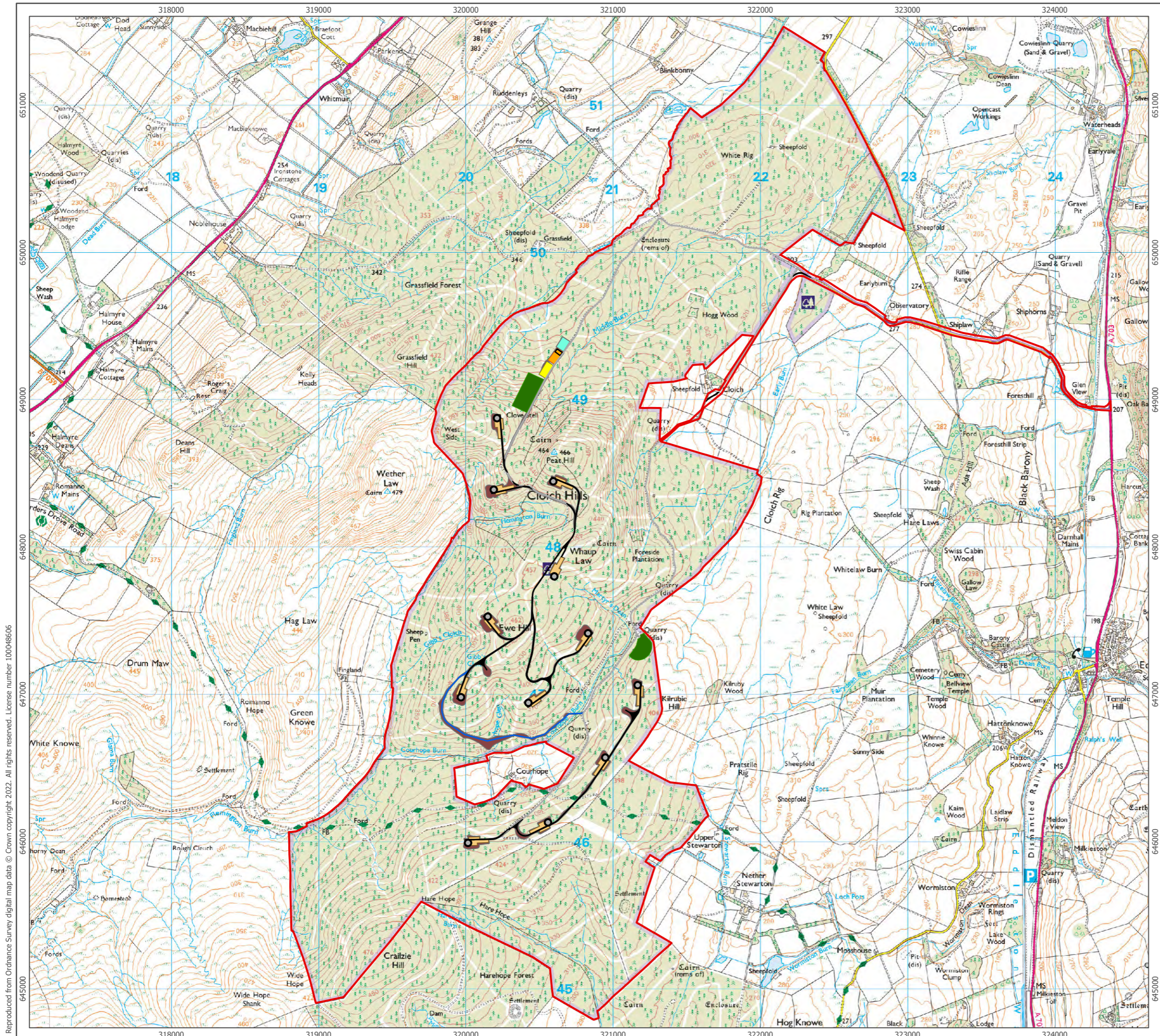
The findings of the probing indicate that the majority of the Development is underlain by peat at a depth of less than 0.5 m. While pockets of deep peat were recorded during the peat probing, these areas were out with the footprint of the Development.

Based on the scope of the study, the PSRA has indicated that the entire Site is 'negligible or low' hazard ranking with half of the hazard zones ranked as 'low' hazard ranking.

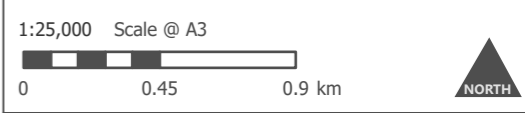
The relocation of T8 and addition of the Scottish Power Transmission TCC have not resulted in any additional peat slide risk with both located in zones of 'negligible' hazard ranking.

Notwithstanding the findings of the PSRA, the final design of infrastructure should be carefully sited and micro-siting adopted if required in order to maintain the design objective of avoiding potential peat slide risk.

## **APPENDIX A - FIGURES**



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound

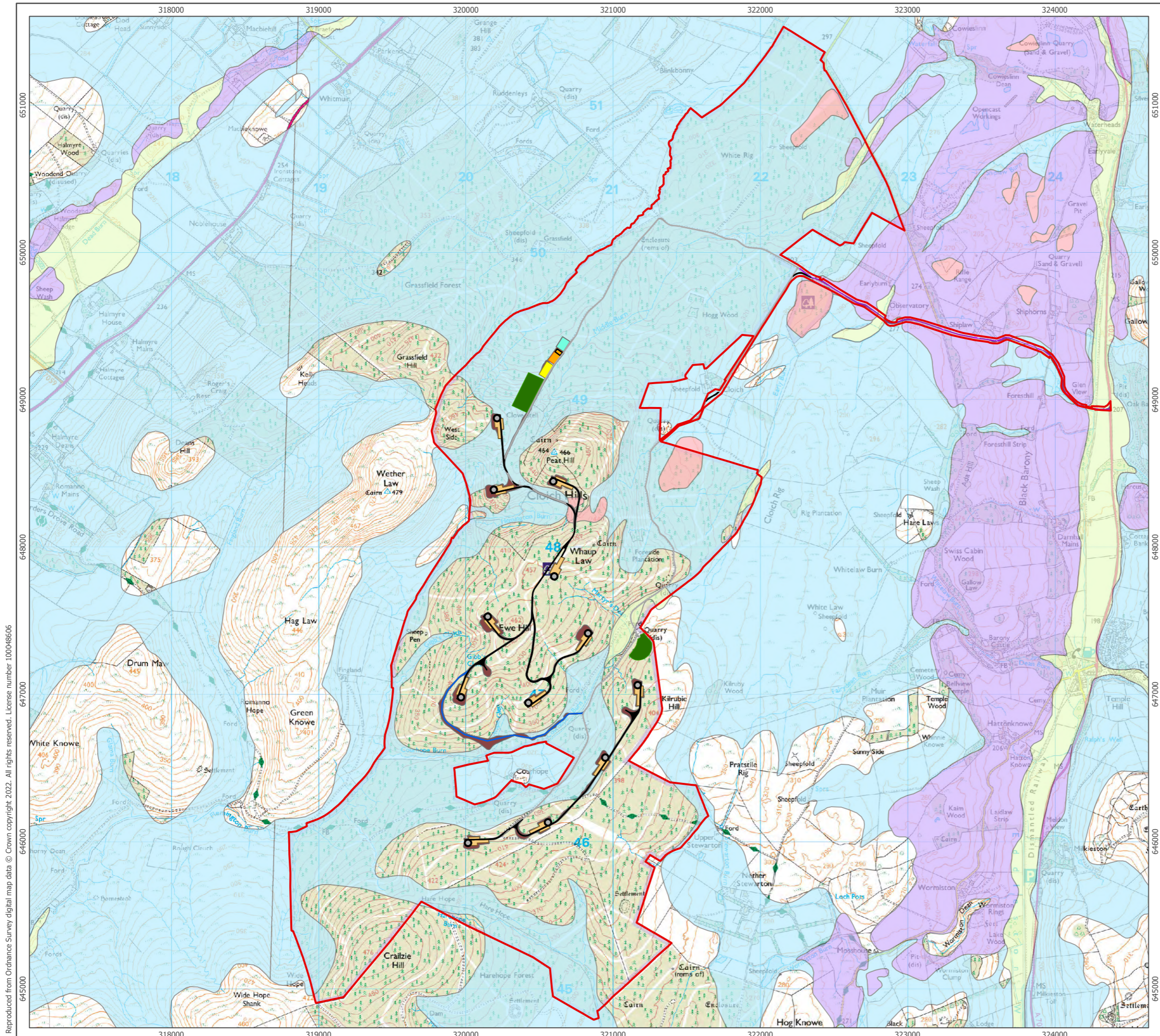


Produced By: CS	Ref: 4519-REP-002
Checked By: DB	Date: 11/17/2022

**Site Layout Plan**  
Figure 9.1.1



**Cloich Forest Wind Farm SEI  
Technical Appendix 9.1:  
Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Superficial Soils**
- ALLUVIUM
- GLACIOFLUVIAL DEPOSITS
- PEAT
- TILL, DEVENSIAN

1:25,000 Scale @ A3

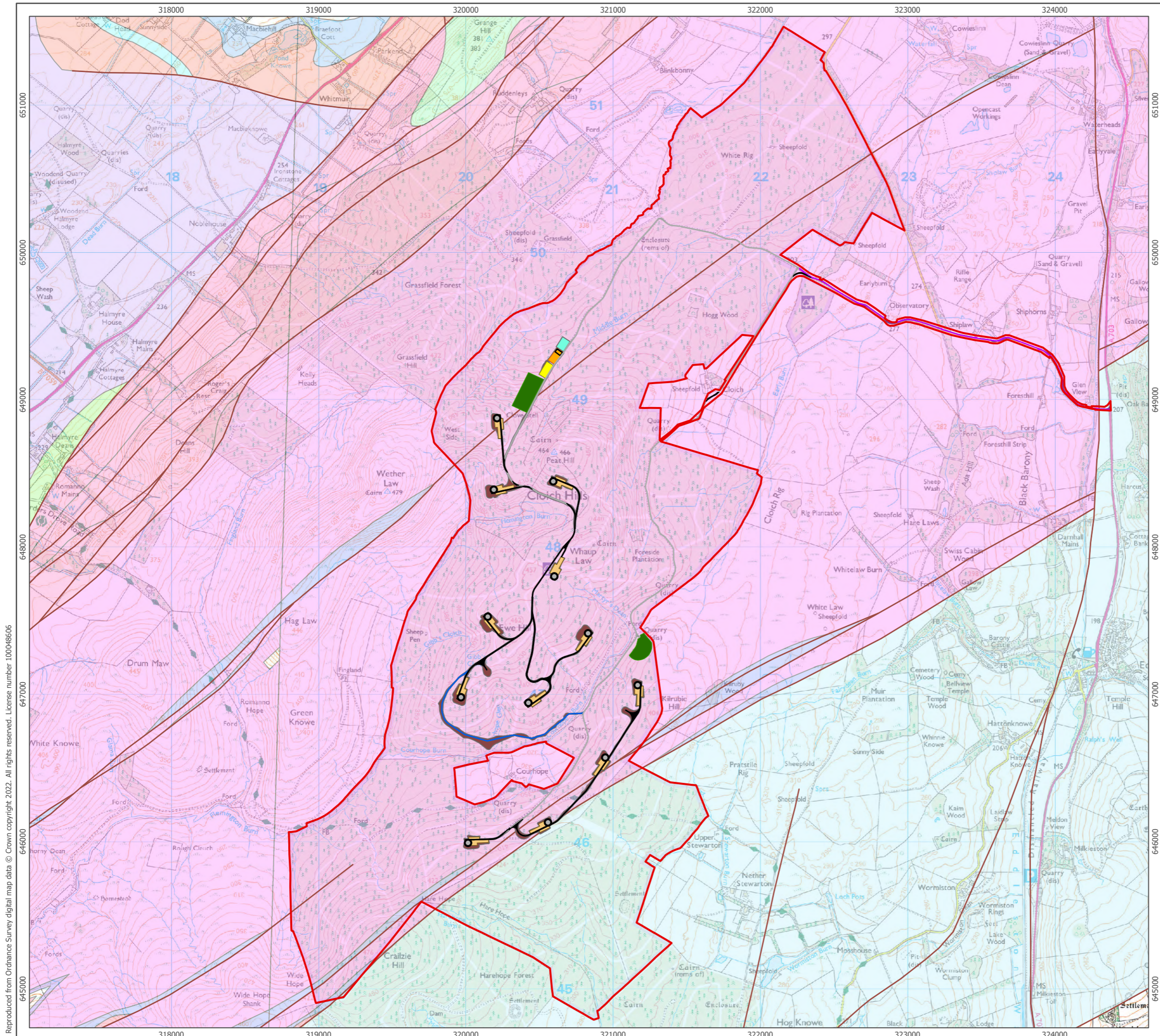



Produced By: CS	Ref: 4519-REP-003
Checked By: DB	Date: 11/17/2022

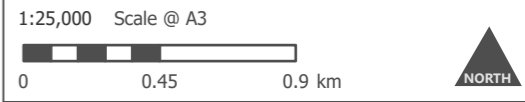
**Superficial Soils**  
Figure 9.1.2

**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Faults**
- Faults
- Bedrock Geology**
- AUCHTITENCH SANDSTONE FORMATION
- BIGGAR VOLCANIC FORMATION
- CLYDE PLATEAU VOLCANIC FORMATION
- CRAWFORD GROUP
- HURLET LIMESTONE
- KIRKCOLM FORMATION
- LAMANCHA CONGLOMERATE FORMATION
- LIMESTONE COAL FORMATION
- LOWER HARTFELL SHALE FORMATION
- MARCHBURN FORMATION
- MOFFAT SHALE GROUP
- PORTPATRICK FORMATION
- STRATHCLYDE GROUP



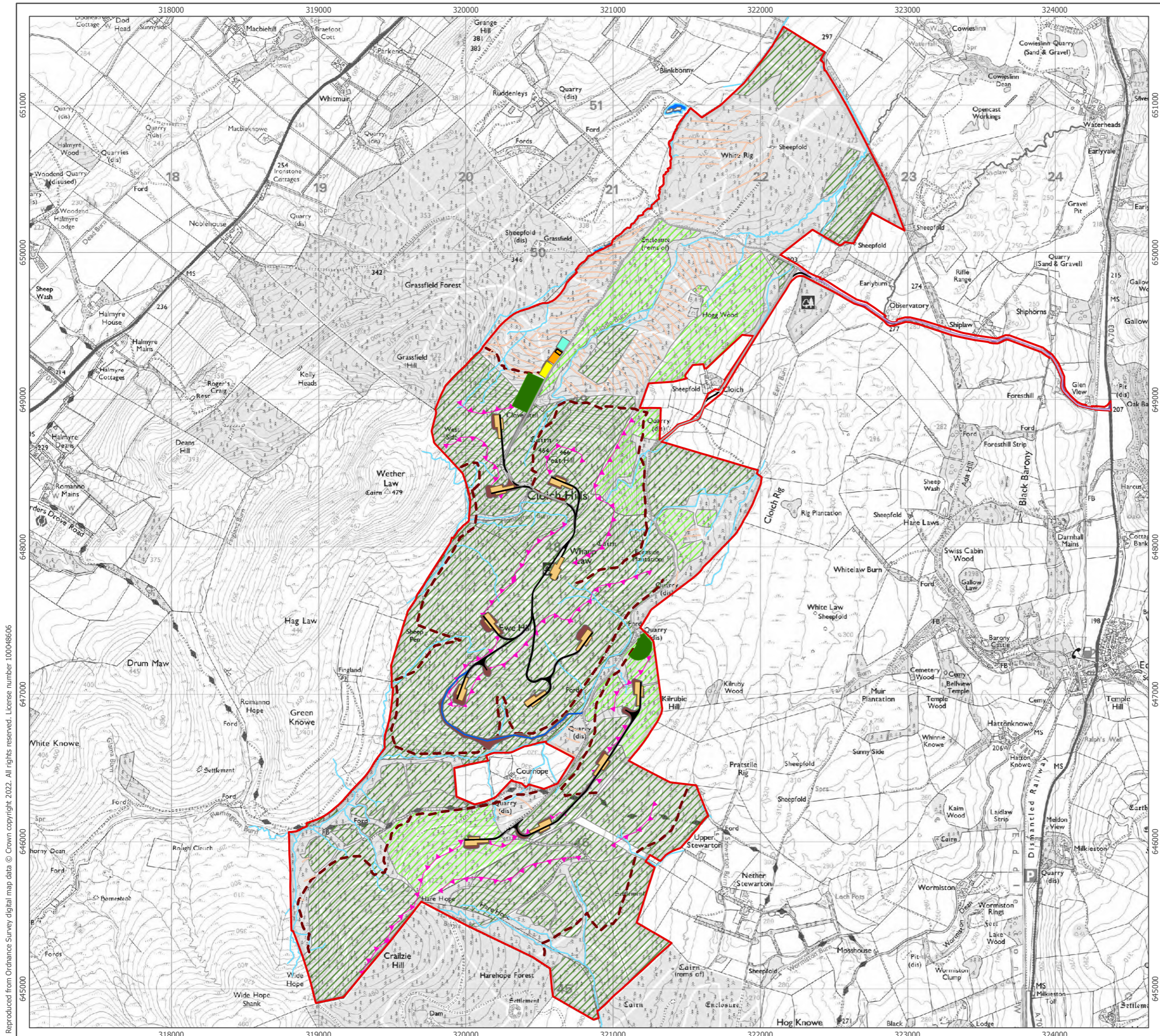
Produced By: CS	Ref: 4519-REP-004
Checked By: DB	Date: 11/17/2022

**Solid Geology**  
Figure 9.1.3



**Cloich Forest Wind Farm SEI  
Technical Appendix 9.1:  
Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606





- Site Boundary
- Turbine Locations
- Artificial Drainage
- Bottom of Slope
- Top of Slope
- Watercourses
- Young Forestry
- Mature Forestry
- Body of Water
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound

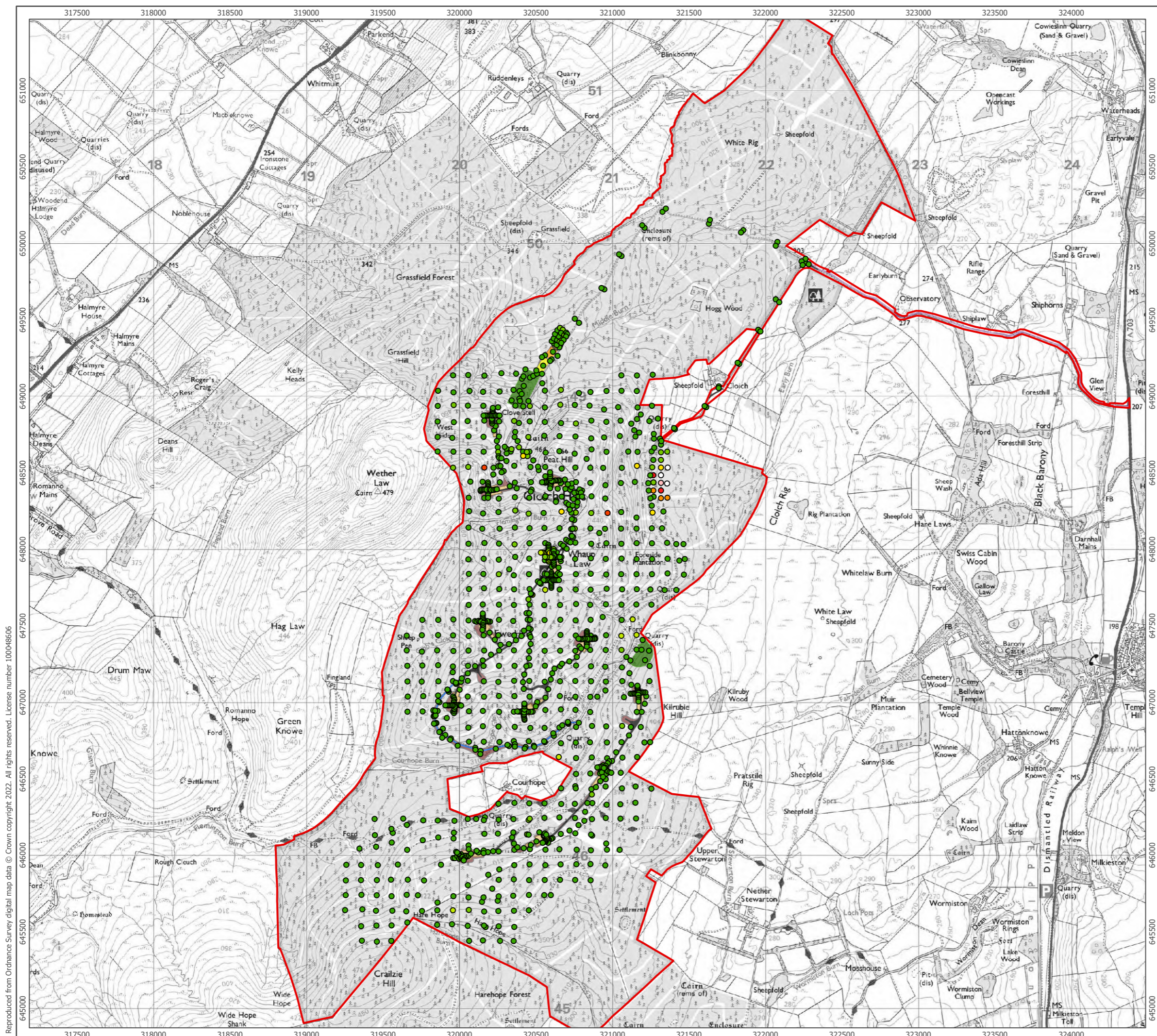
1:25,000 Scale @ A3  
  


Produced By: CS	Ref: 4519-REP-005
Checked By: DB	Date: 11/17/2022

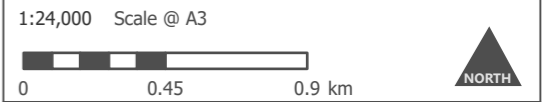
**Geomorphology Map**  
Figure 9.1.4

**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Peat Depth (m)**
- 0.00 - 0.50
- 0.51 - 1.00
- 1.01 - 1.50
- 1.51 - 2.00
- 2.01 - 2.50
- 2.51 - 3.00
- 3.01 - 3.50
- 3.51 - 4.00
- 4.01 +

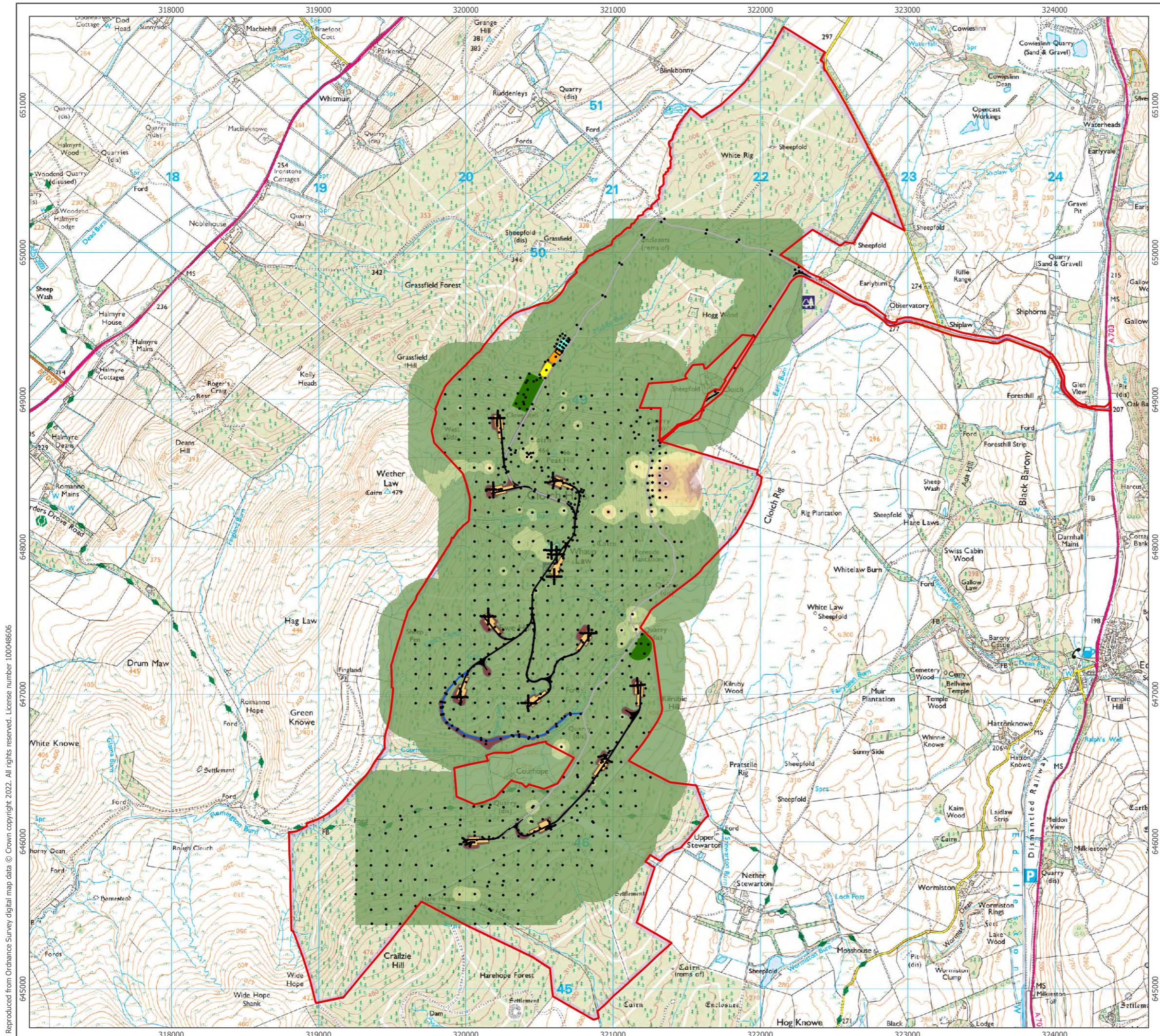


Produced By: CS	Ref: 4519-REP-006
Checked By: DB	Date: 11/17/2022

**Recorded Peat Depths**  
Figure 9.1.5

**Cloich Forest Wind farm SEI**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



**Site Boundary**

- Peat Probe Locations

**Site Infrastructure**

- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound

**Peat Depths (m)**

- 0.00 - 0.50
- 0.51 - 1.00
- 1.01 - 1.50
- 1.51 - 2.00
- 2.01 - 2.50
- 2.51 - 3.00
- 3.01 - 3.50
- 3.51 - 4.00
- 4.01 +

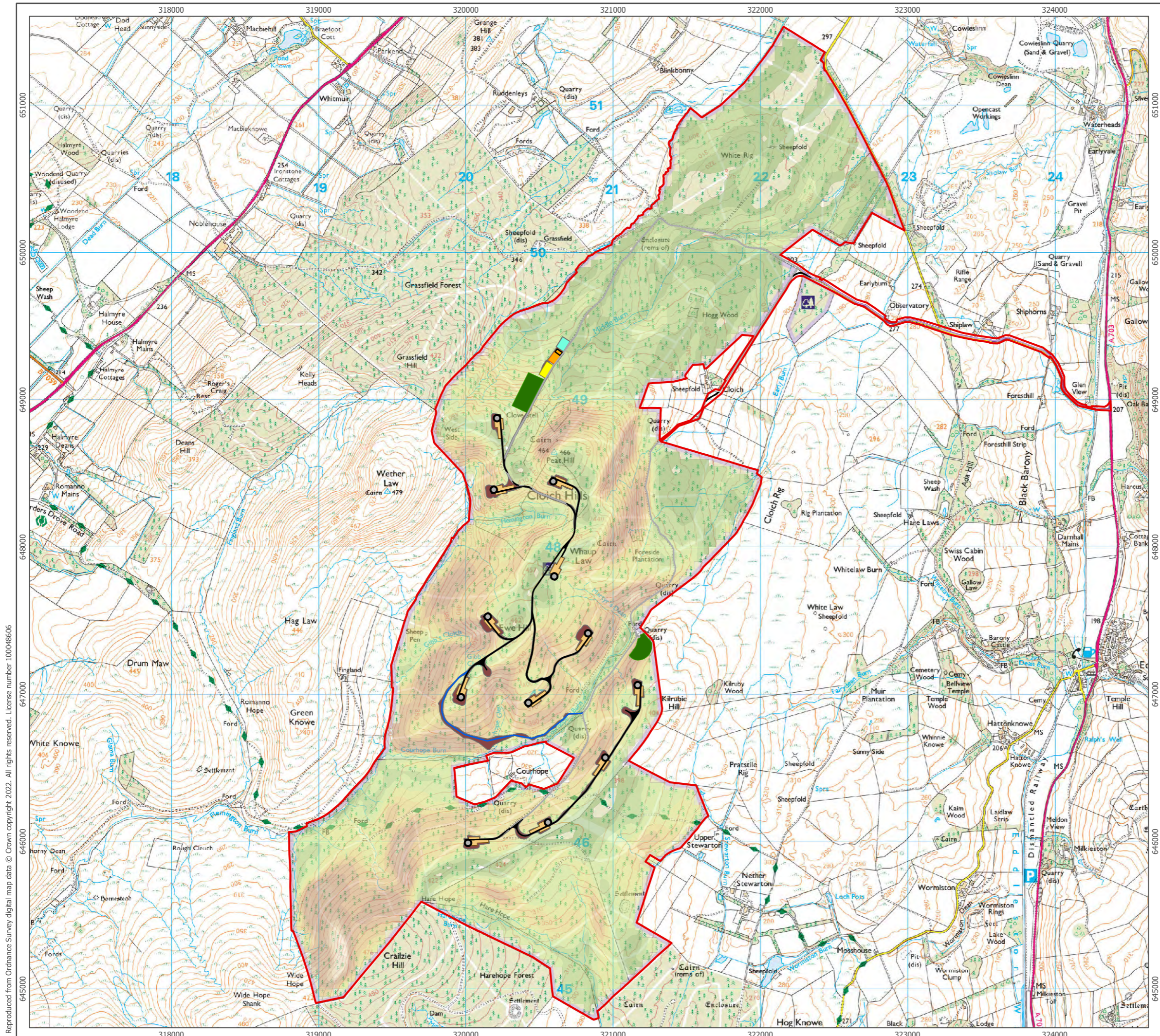
1:25,000 Scale @ A3

Produced By: CS	Ref: 4519-REP-007
Checked By: DB	Date: 11/17/2022

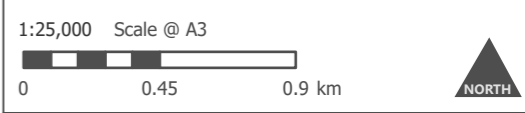
**Interpolated Peat Depths**  
Figure 9.1.6

**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Slope Gradient (deg)**
- 0.00 - 2.00
- 2.01 - 4.00
- 4.01 - 6.00
- 6.01 - 8.00
- 8.01 - 10.00
- 10.01 - 12.00
- 12.01 - 14.00
- 14.01 - 16.00
- 16.01 - 18.00
- 18.01 - 20.00
- 20.01 - 22.00
- 22.01 - 24.00
- 24.01 - 26.00
- 26.01 - 28.00
- 28.01 - 30.00

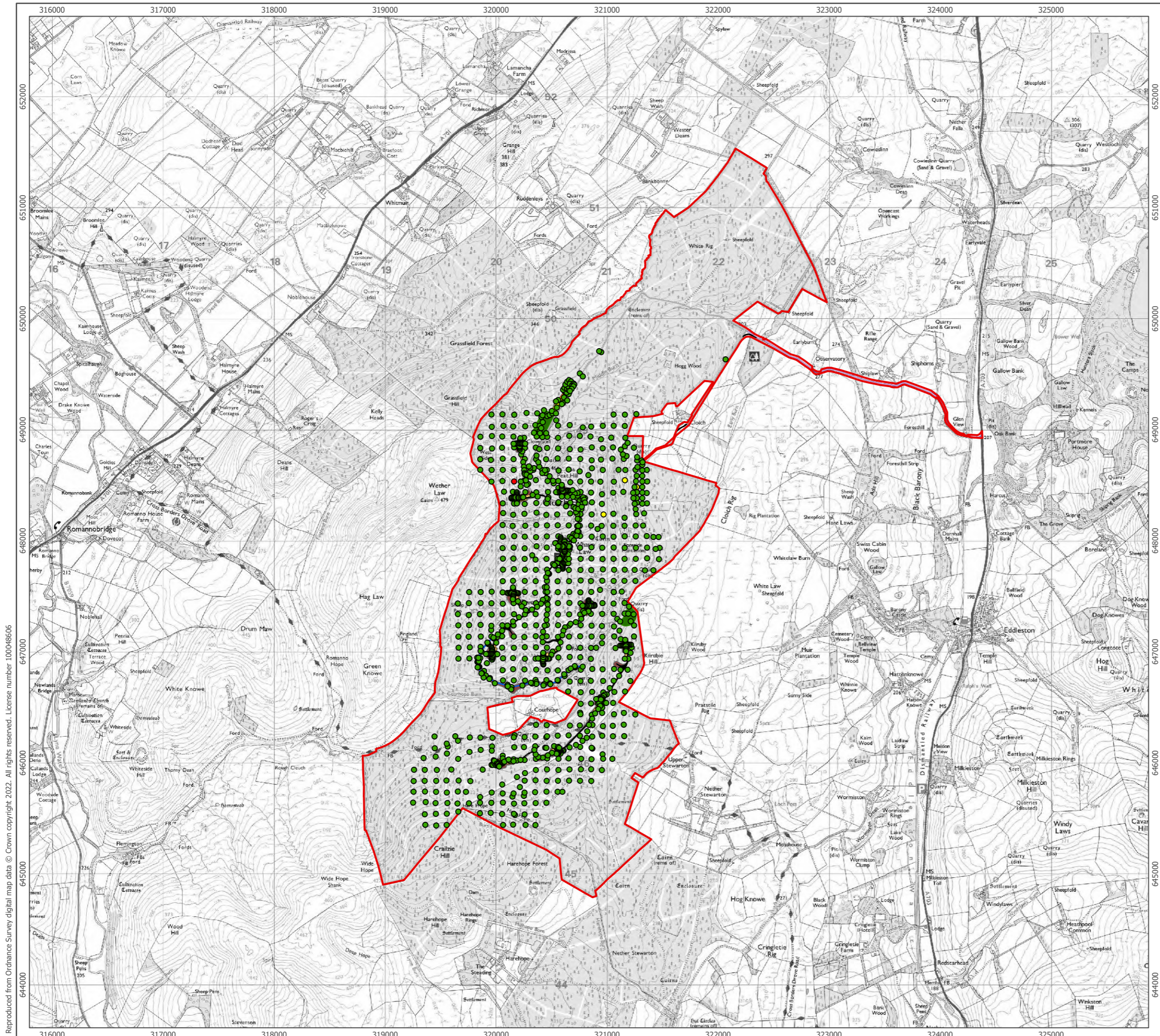


Produced By: CS	Ref: 4519-REP-008
Checked By: DB	Date: 11/17/2022

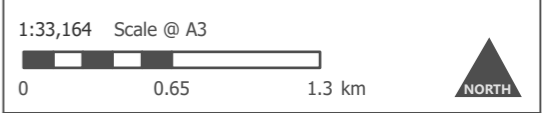
**Slope Gradient**  
Figure 9.1.7

**Cloich Forest Wind Farm**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Factor of Safety**
- Low
- Medium
- High

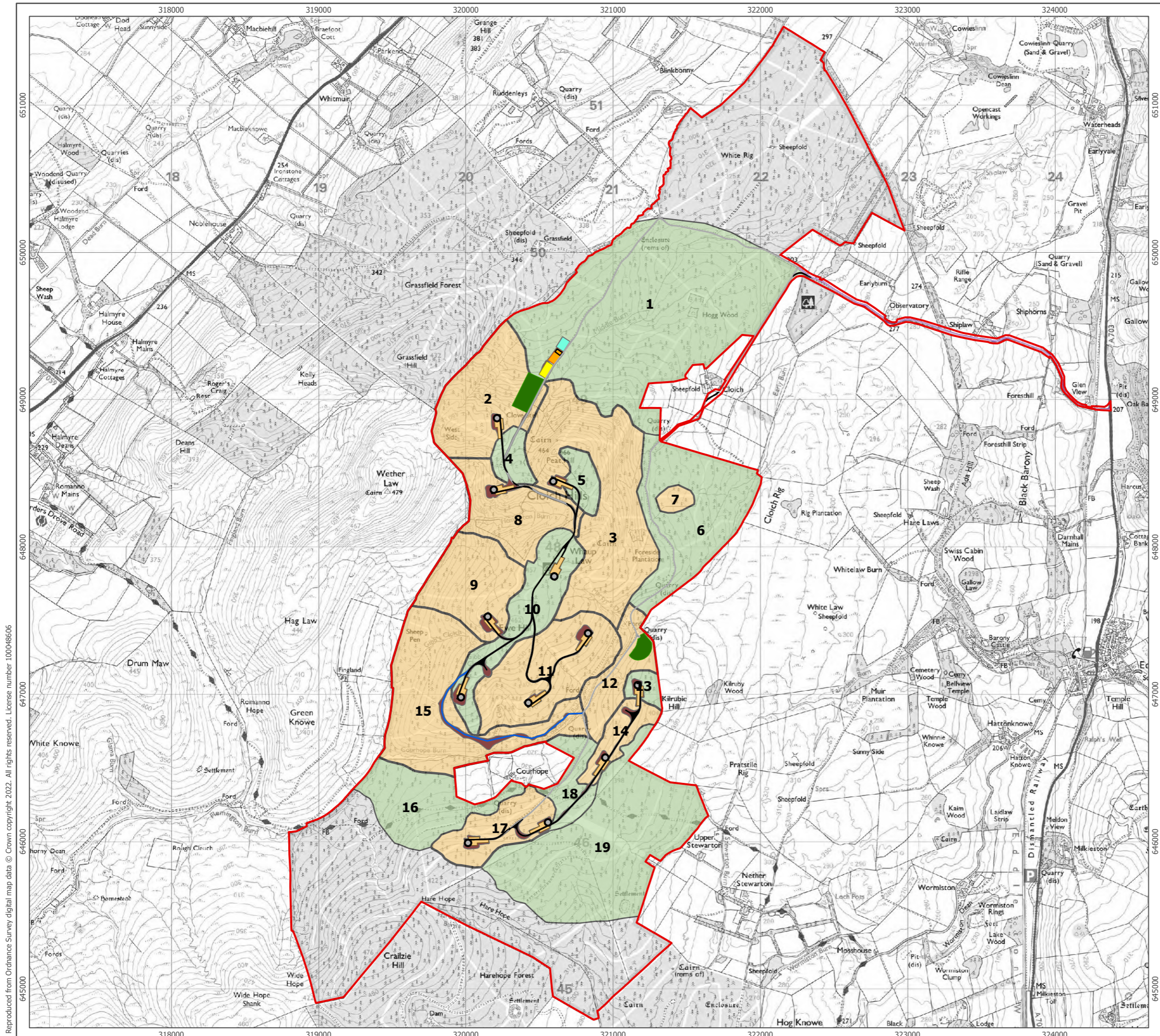


Produced By: CS	Ref: 4519-REP-009
Checked By: DB	Date: 11/17/2022

**Factor of Safety Plan**  
Figure 9.1.8



**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Hazard Ranking Zones**
- Negligible
- Low

1:25,000 Scale @ A3

Produced By: CS	Ref: 4519-REP-010
Checked By: DB	Date: 11/17/2022

**Hazard Ranking Zonation Plan**  
Figure 9.1.9

**Cloich Forest Wind Farm**  
**Technical Appendix 9.1:**  
**Peat Slide Risk Assessment**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606

## **APPENDIX B - SITE PHOTOGRAPHS**

*Photograph 1 - View North along existing track in the Southern Site area*



*Photograph 2 – Sphagnum mosses in clearing within the central Site area*



***Photograph 3 – View Southeast from the central Eastern Site area***



***Photograph 4 – Existing quarry along North western Site access***





*Photograph 5 – Fire break within plantation in the western Site area*



*Photograph 6 – Engineered track through plantation in the western Site area*



*Photograph 7 – View North from central area of the Site*



*Photograph 8 – Watercourse running through plantation in the central Western Site area*



## **APPENDIX C – HAZARD RANK ASSESSMENT RECORDS**



















# ARCUS

**CLOICH FOREST WIND FARM  
SUPPLEMENTARY ENVIRONMENTAL  
INFORMATION**

**VOLUME 3: SEI REPORT TECHNICAL APPENDICIES**

**TECHNICAL APPENDIX A9.2:  
OUTLINE PEAT MANAGEMENT PLAN**

**NOVEMBER 2022**



Prepared By:

**Arcus Consultancy Services**

7<sup>th</sup> Floor  
144 West George Street  
Glasgow  
G2 2HG

**T** +44 (0)141 221 9997 | **E** [info@arcusconsulting.co.uk](mailto:info@arcusconsulting.co.uk)  
**w** [www.arcusconsulting.co.uk](http://www.arcusconsulting.co.uk)

Registered in England & Wales No. 5644976

## TABLE OF CONTENTS

<b>1</b>	<b>INTRODUCTION .....</b>	<b>1</b>
<b>2</b>	<b>OBJECTIVES .....</b>	<b>3</b>
<b>3</b>	<b>PEAT INVESTIGATIONS, EXCAVATION, RE-USE AND MANAGEMENT .....</b>	<b>7</b>
<b>4</b>	<b>CONCLUSION.....</b>	<b>13</b>
	<b>APPENDIX A - FIGURES.....</b>	<b>14</b>
	<b>APPENDIX B – CALCULATIONS .....</b>	<b>15</b>

## 1 INTRODUCTION

### 1.1 Background

Arcus Consultancy Services Ltd (Arcus) were commissioned by Cloich Windfarm Partnership LLP, wholly owned by EDF Energy Renewables UK Limited, ('the Applicant') to carry out an Outline Peat Management Plan (oPMP) for the amendments to the proposed Cloich Forest Wind Farm (the SEI Layout) for the proposed Cloich Forest Wind Farm ('the Development') located in the Scottish Borders, centred at approximately (NGR) 320648, 647881, 5.5 kilometres (km) north-west of Peebles ('the Site').

This Supplementary Environmental Information (SEI) Report provides further, and updated, environmental information in light of revisions to the Development. The Applicant has revised the Development by:

- Relocating Turbine 8 (T8) and its associated infrastructure to ensure that it is sufficiently removed from Whaup Law Cairn;
- Provision for an additional control building at the substation compound. It is expected that the grid operator (SPT) will request a separate control building to the wind farm's control building.
- The addition of a new SPT Temporary Construction Compound (TCC) in the north of the Site.

Additional felling is required for due to these changes. This oPMP will provide estimated peat excavation and re-use potential, and the proposed peat and soils management methodologies to be employed during construction of the Development.

This oPMP has been prepared to be a Technical Appendix to **Chapter 9: Geology, Ground Conditions & Peat** of the SEI Report. This oPMP will ensure the Development complies with good practice in accordance with Scottish Renewables (SR) and Scottish Environment Protection Agency (SEPA) guidance.

The purpose of the oPMP is to:

- Define the materials that will be excavated as a result of the Development, focusing specifically on the excavation of peat;
- Report on detailed investigations into peat depths within the Development;
- Detail proposals for the management of excavated peat and other soils;
- Consider the potential effect of the Development on Ground Water Dependent Ecosystems (GWDTEs);
- Determine volumes of excavated arisings, the cut/fill balance of the Development and proposals for re-use or reinstatement using excavated materials; and
- Detail management techniques for handling, storing and depositing peat for reinstatement.

The oPMP has been produced in accordance with best practice guidance and legislation as detailed in Section 2.1 of this oPMP. This oPMP is intended to be a document that will evolve during the different phases of the Development and as such, will be subject to continued review to address:

- Requirements to discharge future Planning Conditions;
- Detailed ground investigations and detailed design of the Development;
- Unforeseen conditions encountered during construction;
- Changes in best practice during the operational lifetime of the Development; and
- Changes resulting from the construction methods used by the Contractor(s).

Whilst this oPMP provides a base standard for good practice, where avoidance or further minimisation of risks to the environment can be demonstrated through use of alternative methods or improvements to current practices, the Contractor (once appointed) will

implement these wherever possible and will correspond with SEPA and Scottish Borders Council ('the Council').

This oPMP is accompanied by the following appendices:

- Appendix A – Figures; and
- Appendix B – Peat Excavation and Re-use Calculations.

## 1.2 The Site

The land within the site boundary ('the Site') which contains the turbines and associated infrastructure covers an area of 1,080 hectares (ha), centred on National Grid Reference (NGR) 320648, 647881. The Site is located approximately 5.5 km north-west of Peebles. The Site is located wholly within the administrative boundary of the Scottish Borders Council and lies adjacent to the A703 on the east side of the Site.

The topography of the Site and the immediate vicinity is complex, with elevations ranging from approximately 280 m Above Ordnance Datum (AOD) in the north-east part of the Site to approximately 476 m AOD at the peak of Craillie Hill in the south. The Site encompasses the rolling Cloich Hills, including Peat Hill (466m AOD), Ewe Hill (462m AOD), White Rig (325m AOD), and Craillie Hill (476m AOD). The hills are dissected by a number of watercourses, including Middle Burn, Flemington Burn, Martyr's Dean, Courhope Burn and Harehope Burn. All watercourses eventually feed into the River Tweed. There are no waterbodies within the Site.

Coniferous plantation, at various stages of the planting, growing and felling cycle, is the primary land use within the Site; however the area around Courhope in the south of the Site consists of improved upland pasture, utilised for sheep grazing, and improved grassland which remains clear of forestry.

In addition to the operational commercial forest of Cloich Forest, the Site and immediate vicinity consists of further areas of forestry and rural farmland, primarily used for grazing and other farmland activities.

The Site contains two public roads which form the Site access from the A703; these public roads are as follows:

- D17 Whim – Shiplaw; and
- D18 Cloich.

There are no residential properties within the Site; however, Cloich Farm is located adjacent to the Site, at approximate NGR 321655, 649105, approximately 1.2 km north-west from the closest turbine (T10).

## 1.3 The Development

The revised Development will consist of the following key infrastructure:

The SEI Layout is illustrated in Figure 9.2.1 in Appendix A of this oPMP and will consist of the following key infrastructure with changes incorporated within the SEI Layout shown in bold:

- Up to 12 wind turbines three-bladed turbines, **including the relocation of T8 150 m to the south**, with a maximum tip height of up to 149.9 m;
- Widening works along public roads 'D17 Whim – Shiplaw' & 'D18 Cloich';
- Access tracks linking the turbine locations;
- Network of underground cabling running adjacent to the access tracks where possible;
- Substation compound incorporating **two** single storey control **buildings**, external electrical infrastructure, BESS components, recycling and storage, and vehicle parking etc.;

- Crane hardstandings and an external transformer for each turbine;
- Temporary Construction Compound (TCC);
- Two Borrow Pits;
- **Scottish Power Transmission (SPT)TCC.**
- An approximate 20 MW battery energy storage system (BESS); and
- Forestry felling, **including an additional area required due to the relocation of T8 and additional TCC.**

## 1.4 Consultation

Peat management within the Site, both excavation/disturbance and the reinstatement /restoration, was considered throughout the EIA for the Development and the outcomes of studies are reported in the EIA Report. The EIA Report forms part of the planning application submitted to the Scottish government's Energy Consent Unit (ECU) and made available to all consultees, including SEPA.

Further consultation beyond scoping took place between Arcus and SEPA regarding the methodology for investigating the peat depths during the Phase 2 Peat Probing. SEPA acknowledged the approach proposed and highlighted the need for the Development to avoid the deepest peat areas where possible and the requirement for detailed peat probing. This oPMP considers assessments included in the EIA Report while responding to the consultees scoping responses.

Considerations given to the management of peat during the EIA were also applied to the revisions made to the design within the SEI Layout. Additional peat probing was carried out at the revised location of T8 and additional TCC location. This survey followed the same methodology as was used in the EIA phase 2 peat probing survey. The results gathered supplemented the EIA survey results to assess the volume of peat excavated and reinstatement potential for the SEI Layout, included within Appendix B of this oPMP.

SEPA's response to the EIA included a request for a detailed PMP as follows:

*Detailed Peat Management Plan (PMP) to be submitted to the satisfaction of the determining authority in consultation with SEPA; This is to be submitted at least 3 months prior to construction commencing on site and to be agreed with the determining authority in consultation with SEPA.*

*Reason: To ensure minimisation and mitigation of peat disturbance and degradation.*

## 2 OBJECTIVES

### 2.1 Introduction

Desk-based assessments, detailed peat survey work, and completion of technical assessments such as the Peat Slide Risk Assessment (PSRA) for the SEI Report allows a consistent approach for managing peat.

The preparation of an oPMP responds to the 2019 Scoping Responses (Oct 2019 – Dec 2019) and the intent to deliver a construction project that complies with good practice in accordance with SR and SEPA guidance.

In addition to the assessments, an outline civil design of the Development has been undertaken. With respect to geology, ground conditions and peat, the overall objective of the design of the Development has been to minimise the excavation of peat where possible. While the revisions incorporated within SEI Layout were not related to reducing the impacts on geology, ground conditions and peat, consideration of the SEI Layout still required assessment.

Due to the nature of the underlying ground conditions on the Site, tracks were designed to be as close as possible to existing levels. This is considered to provide the best



opportunity for a design which achieves reinstatement or restoration in accordance with good practice and the methods set out in the outline Habitat Management Plan (HMP - as included in **Chapter 7: Ecology** of the EIA Report) while removing the need for off-site waste management controls.

This objective of the oPMP is achieved through:

- Ensuring the characteristics of the Site are understood through extensive peat probing and assessing the Site topography;
- Understanding the extent of SEI Layout and how excavations will take place;
- Modelling the peat depth profile based on probing and a digital terrain modelling in 3D;
- Considering the best practice advice for peat reinstatement; and
- Developing practical peat restoration opportunities for improvement of habitats and peatlands.

This oPMP has been compiled in accordance with the following best practice guidance:

- Guidance on Developments on Peatland: Peatland Survey<sup>1</sup>;
- Guidance on Developments on Peatland: Guidance on the Assessment of Peat Volumes, Re-use of Excavated Peat and Minimisation of Waste<sup>2</sup>;
- Floating Roads on Peat Guidance<sup>3</sup>;
- Good Practice During Wind Farm Construction<sup>4</sup>; and
- SEPA Regulatory Position Statement – Developments on Peat<sup>5</sup>.

## 2.2 Approach to Minimising Peat Excavation

The following steps have been taken during the development of the design of the SEI Layout to minimise the effect on peat:

- The development of an access track design which avoids any deeper peat where practicable; and
- The design and orientation of turbines and crane hardstandings considering local topographical, peat and other environmental constraints.

These steps will be further supplemented by taking the following measures to minimise disturbance:

- Maximisation of batter angles in cuttings;
- Utilisation of existing tracks; and
- The use of appropriate construction plant to avoid unnecessary disturbance of the ground surface.

The fundamental principle upon which this oPMP is based is that achieving a successful materials strategy is contingent on gaining a thorough understanding of the Site through investigation and developing a design that achieves the materials management

---

<sup>1</sup>SNH (2017) Guidance on Developments on Peatland: Peatland Survey (2017) [Online] Available at: <https://www.gov.scot/binaries/content/documents/govscot/publications/advice-and-guidance/2018/12/peatland-survey-guidance/documents/peatland-survey-guidance-2017/peatland-survey-guidance-2017/govscot%3Adocument/Guidance%2Bon%2Bdevelopments%2Bon%2Bpeatland%2B-%2Bpeatland%2Bsurvey%2B-%2B2017.pdf> (Accessed 05/05/21)

<sup>2</sup> Scottish Government (2014) Assessment of Peat Volumes, Reuse of Excavated Peat and Minimisation of Waste [Online] Available at: <https://www.gov.scot/publications/assessment-of-peat-volumes-reuse-of-excavated-peat-and-minimisation-of-waste-guidance/> (Accessed 05/05/21)

<sup>3</sup> SNH (2010) Floating Roads on Peat [Online] Available at: <http://www.roadex.org/wp-content/uploads/2014/01/FCE-SNH-Floating-Roads-on-Peat-report.pdf> (Accessed 05/05/21)

<sup>4</sup> Scottish Renewables et al. (2019) Good Practice during Wind Farm Construction [Online] Available at: <https://www.nature.scot/sites/default/files/2020-12/Good%20Practice%20during%20wind%20farm%20construction%20-%204th%20Ed.pdf> (Accessed 05/05/21)

<sup>5</sup> SEPA (2010) SEPA Regulatory Position Statement – Developments on Peat [Online] Available at: [https://www.sepa.org.uk/media/143822/peat\\_position\\_statement.pdf](https://www.sepa.org.uk/media/143822/peat_position_statement.pdf) (Accessed 05/05/21)

objectives. For the Development, this principle is achieved by undertaking significant peat probe investigations prior to preparing the outline civil engineering design layout in 3D and the development of this oPMP based on the available information.

## 2.3 Aims and Objectives

### 2.3.1 *Need for a Peat Management Plan*

The significance of peatlands is most evident in their protection by various legislation, policy and local, national or international initiatives including but not limited to;

- United Kingdom Biodiversity Action Plan (UKBAP)<sup>6</sup>;
- Scotland's National Peatland Plan (SNH, 2015)<sup>7</sup>;
- European Council Habitats Directive 92/43/EEC (Council of the European Communities, 1992)<sup>8</sup>;
- Scottish Biodiversity List (SBL) (Scottish Government, 2013)<sup>9</sup>;
- Scottish Government discussion paper on the Management of Carbon-Rich Soils (Scottish Government, 2010)<sup>10</sup>;
- Scottish Soil Framework (Scottish Government, 2009)<sup>11</sup>; and
- Climate Change Plan (2017-2032) (Scottish Government et al., 2017)<sup>12</sup>.

SEPA has a statutory and legislative duty to ensure that where peat spoil is generated during construction, it is stored, re-used, treated or disposed of correctly, which may require authorisation or permits.

SEPA's policy on the management of peat is set out within SEPA Regulatory Position Statement – Developments on Peat<sup>13</sup>. This highlights that the best management option for peat spoil is the prevention of its production, by seeking to minimise peat excavation and disturbance. Where this is unavoidable, developers should attempt to re-use as much of the peat produced on-site as is possible, in justifiable and environmentally beneficial ways.

This oPMP is prepared to demonstrate to the Council, SEPA, and other consultees that the construction of the Development will progress in a manner that is planned, in accordance with good practice, and achieves the aim of being environmentally sustainable.

This oPMP is therefore prepared in accordance with the SR and SEPA guidance. It details how:

- The Development has been structured and designed so far as practicably possible to reduce the volumes of peat excavated;
- Volumes of peat excavated during the course of the works have been considered in the design; and
- Excavated peat will be managed.

---

<sup>6</sup> <https://jncc.gov.uk/our-work/uk-bap/>

<sup>7</sup> <https://www.nature.scot/scotlands-national-peatland-plan-working-our-future>

<sup>8</sup> <https://www.legislation.gov.uk/eudr/1992/43/contents>

<sup>9</sup> <https://www.nature.scot/scotlands-biodiversity/scottish-biodiversity-strategy/scottish-biodiversity-list>

<sup>10</sup> <https://www.gov.scot/publications/low-carbon-scotland-meeting-emissions-reduction-targets-2010-2022-report/pages/10/>

<sup>11</sup> <https://www.gov.scot/publications/scottish-soil-framework/>

<sup>12</sup> <https://www.gov.scot/publications/draft-climate-change-plan-draft-third-report-policies-proposals-2017/>

<sup>13</sup> SEPA Regulatory Position Statement – Developments on Peat [Microsoft Word - Peat Position Statement - update 290310.doc \(sepa.org.uk\)](#)

### **2.3.2 Objectives of the oPMP**

The main objective of the oPMP is to outline how peat and peaty soils proposed to be excavated will be managed and re-used during the construction of the Development and proposed restoration plans.

This is achieved through responding of the following objectives:

- Providing details of the extent and depth of the peat on Site and how this was determined;
- Estimation of peat volumes to be excavated and re-used;
- Classification of excavated materials;
- Consideration of the use of appropriate construction methods;
- Describing how excavated peat will be handled to ensure suitability for re-use;
- Determining if temporary storage of peat will be required during construction and how this will be done to ensure suitability for re-use; and
- Considering the potential volume of peat which may not be suitable for re-use and any requirement for a Waste Management Plan for the Development.

The response to these objectives is provided in the following sections.

### **3 PEAT INVESTIGATIONS, EXCAVATION, RE-USE AND MANAGEMENT**

#### **3.1 Peat Classification and Published Geology**

##### **3.1.1 General Peat Classification**

Acrotelmic peat is the upper layer of peat consisting of living and partially decayed materials with a higher hydraulic conductivity and a variable water table. These deposits are generally found to exist in the upper 0.5 m of peat deposits and are typically suitable for reinstatement because they contain viable plant life to assist in the regeneration of peatland vegetation and carbon sequestration.

Catotelmic peat is variable in characteristics, with decomposition of fibres generally increasing with depth. Water content can be highly variable and affects the structural strength of the material. Suitability for re-use generally depends on fibre and water content. The upper catotelm is commonly deemed as being appropriate for re-use in restoration due to its relatively high fibre content.

Generally, excavated semi fibrous catotelmic peat from the Site will have sufficient structural strength to be able to be used in the lower layers of verge restoration as it will not be 'fluid'.

The catotelmic peat would be capped with a surface layer of actrotelm to re-establish the peat vegetation. If any fluid like wet catotelmic peat is encountered then it would be placed in more appropriate locations such as low-lying section of the borrow pits or concave deposition areas.

The following assumptions have been made in classifying peat excavated during the construction work:

- Where the total peat depth was found to be less than 0.5 m, this peat material is assumed to be 100% acrotelmic;
- Where the total peat depth is between 0.5 m and 1.0 m, the upper acrotelmic peat is at least 0.5 m deep; and
- Where the total peat depth is found to be greater than 1.0 m, acrotelmic peat is assumed to account for at least 30% of total depth but generally applying minimum of 0.5 m thick.

Existing topography and permitted track gradients drive the design of the infrastructure with due consideration given to potential construction risk and effects on environmentally sensitive receptors including deep peat, watercourse buffers and any GWDTEs. Further micro-siting post-consent would take place in such a way as to avoid where possible the excavation of deep peat.

##### **3.1.2 Published Geology**

Available British Geological Survey (BGS) mapping indicates a large proportion of the Site to be devoid of superficial soils while the remainder of site is underlain almost entirely by Devensian Till, with two small localised pockets of peat in the centre of the Site and to the east in areas which are topographically flatter than their surrounds.

Published bedrock geology mapping indicates the entire Site to be underlain by Wacke (a variety of Sandstone?) of the Kirkcolm Formation. No faulting exists on the Site.

##### **3.1.3 Investigations**

The existing peat depths across the Site have been determined through a phased survey approach. The survey was initiated to inform the EIA, subsequent SEI and design work while supporting the PSRA. The survey comprised a total of 1,129 probes, 1,082 of which

were recorded during the EIA and a further 47 in response to the modifications incorporated within the SEI Layout.

Peat depths ranged from 0 m to 4.6 m thickness across the Site. Areas of deeper peat were shown as localised and isolated zones, with the deepest peat encountered in a pocket situated in the eastern area of the Site. The remainder of deeper pockets of peat were located in the central site area and generally had a depth below 3 m.

Initial Phase 1 peat depth surveys were undertaken in March 2020 comprising a 100 m grid throughout the developable site area, with the exception of areas inaccessible due to dense forestry. This rationale of probing is in accordance with the phase 1 approach as detailed in the Scottish Government guidance for investigating peat.

For the EIA, further peat depth surveys (phase 2a and b) were undertaken across a series of visits between November 2020 and April 2021. The probe positions for this visit were focussed on the proposed turbine, access tracks, and other key infrastructure. Peat depths were measured along the proposed access tracks at 50 m centres with offsets of 25 m on either side of the centre line, and 10 m cross-hair at turbines across the Site. Slight variations to this methodology were necessary due to dense forestry.

Additional peat depth surveys were carried out in June 2022 and August 2022 for the SEI Layout. The updated T8 location was targeted in the first of these surveys, in a crosshair of 10 m centres and probes relating to the associated infrastructure, such as hardstanding and spur track. The additional TCC area was probed in a 25 m x 25 m grid formation during the second additional survey.

The peat depths are illustrated in Figure 9.2.2 - Recorded Peat Depths within Appendix A of this oPMP.

### **3.1.4 Summary of Peat Depths**

Throughout the peat surveys to date, a total of 1,129 probes were progressed. 97% of these probes recorded no peat or peat less than 1.0 m. Thick peat (where the depth was greater than >1.0 m) was recorded at 3% of locations. The majority of thick peat was recorded at depths between 1.0 m – 2.0 m with around 1% of all probes recording depths in excess of 2.0 m. Whilst deep peat was recorded in the 3% of the total probes, the design of the Site layout has avoided impact on these areas.

The maximum peat depth recorded was 4.6 m in the eastern Site area. Generally, deeper peat was encountered in small isolated pockets in areas of flat topography and proposed roads and infrastructure have been avoided in these areas as far as possible.

Peat over the remainder of the Site was typically measured as being less than 0.5 m with the average peat depth across the Site being <0.3 m.

Figure 9.2.3 - Interpolated Peat Depths included in Appendix A.

Prior to commencing works on Site, the Contractor (once appointed), will undertake further ground investigation to establish peat characteristics and surcharging strategies if required.

## **3.2 Excavation and Re-use Calculation**

Excavated peat volumes have been estimated through the production of a peat levels 3D surface derived from the peat depth data from probing survey and compared with a 3D surface developed from the outline civil design of site infrastructure, whilst some assumptions have been adopted.

The estimated peat excavation volumes are included in Table 3.1 using the anticipated construction activities that will generate excavated soils, although it should be noted that the estimates of excavated peat provided in this report are likely to be higher than actually

occur, as micro-siting during construction will allow for the avoidance of localised pockets of deeper peat .

**Table 3.1: Peat Excavation Volumes Based on Construction Activity**

<b>Development Component</b>	<b>Estimated Volume of Excavated Peat (m<sup>3</sup>)</b>	<b>Estimated Volume of Acrotelmic Peat (m<sup>3</sup>)</b>	<b>Estimated Volume of Catotelmic Peat (m<sup>3</sup>)</b>
Turbines and associated earthworks	21,046	21,046	0
New windfarm tracks, turning heads, passing places, existing rack upgrades and associated earthworks	18,239	18,239	0
Construction Compounds	579	579	0
Substation	889	889	0
Borrow Pits	5,234	5,234	0
<b>SUB-TOTAL</b>	<b>45,987</b>	<b>45,987</b>	<b>0</b>
+10% Bulk Factor Contingency	4,599	4,599	0
<b>TOTAL</b>	<b>50,586</b>	<b>50,586</b>	<b>0</b>

A detailed assessment of excavated volumes by location within the Site is provided in Appendix B of this oPMP.

### **3.2.1 Estimation of Peat Re-use Requirements**

The principles of reinstating peat and peat soils should be adhered to for all elements of the infrastructure, comprising of the below:

- Peat and peaty soils will be reinstated on track and infrastructure verges with turves placed on the upper horizons encouraging revegetation;
- All peat, soil and turves excavated from beneath infrastructure will be reinstated in the vicinity of its original location; and
- Restoration activities will be overseen by the Ecological Clerk of Works (ECoW) to ensure methods are properly adhered to.

### **3.2.2 Peatland Restoration Potential**

The outline objectives in proposing utilisation of those presently identified is to:

- Ensure residual volumes of excavated peat from the Development are re-used in areas where ecological benefits and maintained, or increased carbon sequestration can be delivered;
- Promote the re-use of excavated peat materials and avoid their disposal to landfill;
- Promote use of best practices and guidance to ensure that benefit is made from reusing peat and peaty soils for ecological enhancement; and
- Complement planned mitigation identified in the oHMP.

Table 3.2 shows the opportunities for re-use of peat with the Site including the demand for peat re-use, while Table 3.3 summarises the total peat balance estimated during construction of the Development.

**Table 3.2: Peat Re-use Volumes Based on Construction Activity**

<b>Development Area</b>	<b>Total Demand Estimate (m<sup>3</sup>)</b>	<b>Acrotelm Demand (m<sup>3</sup>)</b>	<b>Catotelm Demand (m<sup>3</sup>)</b>	<b>Reinstatement Thickness (max) (m)</b>	<b>Assumptions</b>
Turbines and associated earthworks	18,723.8	18,723.8	0	0.3	Turbines and associated earthworks will be dressed off with up to 0.3m of peat and peaty soils, with catotelm placed in the lower regions and acrotelm and turves placed nearer surface.
New windfarm tracks, turning heads, passing places, existing rack upgrades and associated earthworks	21,911	21,911	0	0.3	Where new windfarm tracks are proposed, peat will be reinstated along verges and associated earthwork banking with peat up to 0.6m thick with verges not expected to exceed 2.5m on either side.
Construction Compounds	1,623.6	1,623.6	0	Up to 0.3	It is assumed that the construction compound will be completely reinstated across the entire disturbed area with peat up to depths of that encountered during any excavations to re-establish the conditions existed previously.
Substation	75	75	0	Up to 0.3	It is assumed that the substation will be reinstated in areas of earthworks banking and verges with peat up to depths of 0.5m, similar to that encountered during any excavations to re-establish the

Development Area	Total Demand Estimate (m <sup>3</sup> )	Acrotelm Demand (m <sup>3</sup> )	Catotelm Demand (m <sup>3</sup> )	Reinstatement Thickness (max) (m)	Assumptions
					conditions existed previously.
Borrow Pits	9,902	9,902	0	Up to 0.3	Peat reinstatement thicknesses will be up to 0.30m
<b>Total</b>	<b>50,586</b>	<b>50,586</b>	<b>0</b>		

Table 3.2 is presented as a summary of the assessment of peat reinstatement volumes. A detailed assessment is provided in Appendix B of this oPMP.

The following assumptions have been made in assessing peat re-use:

- New access track sections assume verges and earthworks on both sides of track with widths of approximately 2.5 m based on topography. As the access track edges will have graded slopes, peat depths will vary across the profile to tie into existing ground levels but are generally assumed not to exceed 0.6 m thick;
- Verges along the access tracks could consist of up to 0.6 m thick peat;
- No peat will be placed on access track verges where the local topography is steep and/or a watercourse is in close proximity;
- Peat will be laid only to a thickness that maintains hydrological conditions to avoid drying out. Peat will not be used as a thin layer or on steeper non-peat slopes. Low verges and landscaping will be formed to permit surface water to drain off the access tracks; and
- Reinstatement at substation and construction compound assumes a maximum peat depth thickness of 0.25 m. This will include the re-use of acrotelmic peat soils and turves.

Peat across the site was relatively thin and no extensive peat excavations will take place. Any excavated peat will be temporarily placed adjacent to where it is excavated, where possible for suitable re-use. It is therefore considered that designated peat storage areas will not be required. These are areas of previous disturbance area where peat was less than 0.5 m, areas out with 50 m buffer of watercourses and where topography permits.

**Table 3.3: Peat Balance Calculations**

Peat Description	Total Peat Demand Estimate for Reinstatement (m <sup>3</sup> )	Total Peat Supply from Excavation (m <sup>3</sup> )	Surplus (+) or Deficit (-) (m <sup>3</sup> )
Acrotelm	50,586	50,586	0
Catotelm	0	0	0
<b>Total</b>	<b>50,586</b>	<b>50,586</b>	<b>0</b>

Table 3.3 demonstrates that all excavated materials will be suitably re-used when adopting the outline approach as detailed above. These volumes should be considered in the context of the total excavated peat during construction. It is likely that balance would be achieved once total excavated peat is established by the appointed Contractor and reinstatement depths are adjusted accordingly.

### 3.2.3 Handling and Storage of Peat

It will be necessary for the Contractor to prescribe methods and timing involved in excavating, handling and storing peat for use in reinstatement. The Contractor will be



responsible for appointing a chartered geotechnical engineer who will monitor any potential stability risks. Construction methods will be based on the following principles, although it should be noted that no catotelmic peat is anticipated to be excavated during the construction of this project, however best practice has been retained should the material arise on site:

- The surface layer of peat (acrotelm) and vegetation will be stripped separately from the catotelmic peat. This will typically be an excavation depth of up to 0.5 m;
- Acrotelmic material will be stored separately from catotelmic material;
- Careful handling is essential to retain any existing structure and integrity of the excavated materials and thereby maximise the potential for excavated material to be re-used;
- Less humified catotelmic peat which maintains its structure upon excavation should be kept separate from any highly humified amorphous or wet catotelmic peat;
- Acrotelmic material will be replaced as intact as possible once construction progresses / as it is complete;
- To minimise handling and transportation of peat, acrotelmic and catotelmic will be replaced, as far as is reasonably practicable, in the locality from which it was removed. Acrotelmic material is to be placed on the surface of reinstatement areas;
- Temporary storage of peat will be minimised, with restoration occurring in parallel with other works;
- Suitable areas should be sited in locations with lower ecological value, low stability risk and at a suitable distance from water courses;
- Reinstatement will, in all instances, be undertaken at the earliest opportunity to minimise storage of turves and other materials;
- Managing the construction work as much as possible to avoid periods when peat materials are likely to be wetter i.e. high rainfall events;
- Temporary storage and replacement of any peat excavated from the borrow pit should occur adjacent to and within the source pit; and
- Transport of peat on Site from excavation to temporary storage and restoration Site should be minimised.

#### ***3.2.4 Waste Management Plan Requirements***

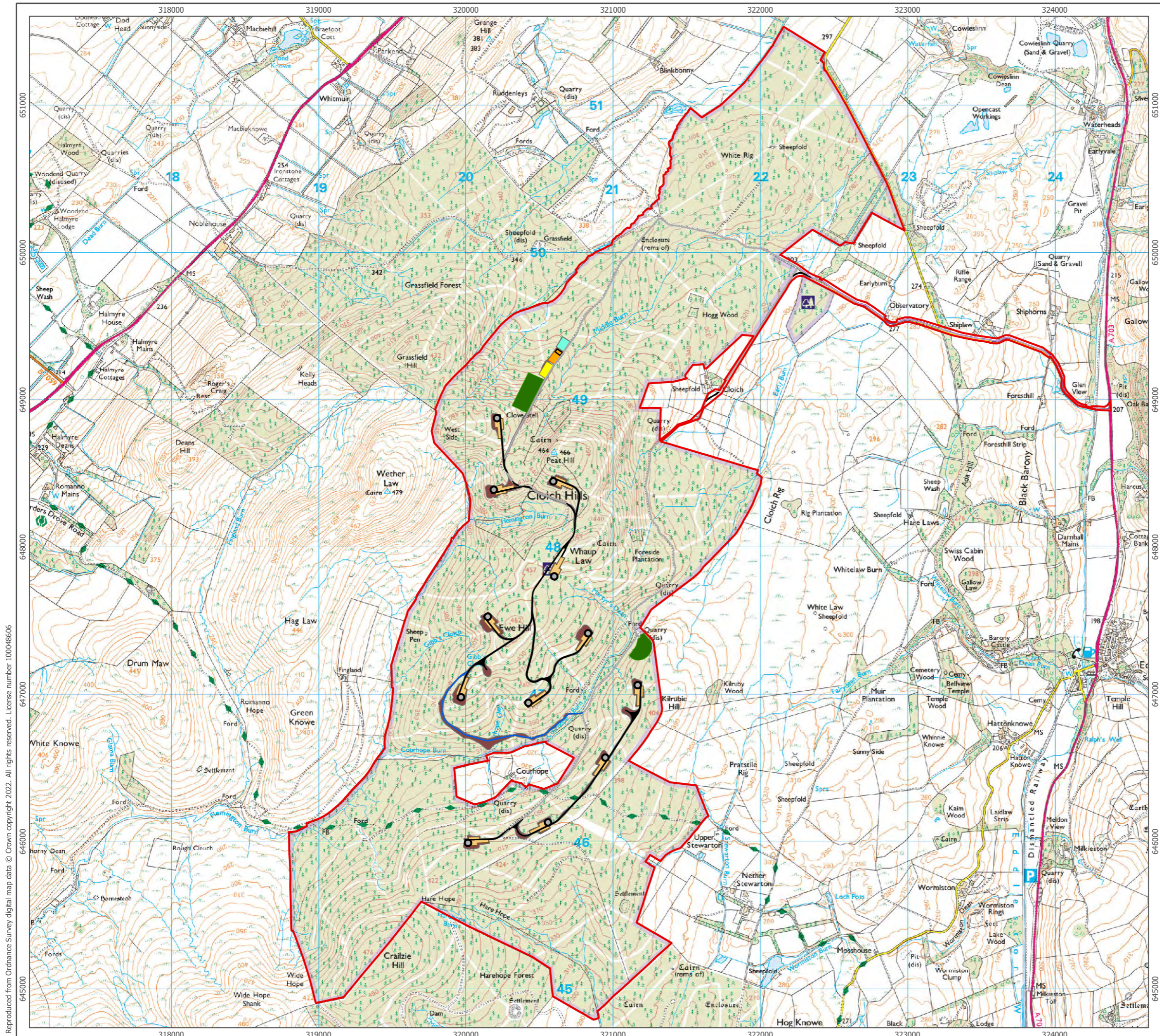
Based on the calculations carried out, the total peat volumes excavated will be fully incorporated in to the reinstatement proposed, therefore waste management and associated licensing in relation to peat does not require further consideration.

#### **4 CONCLUSION**



The following conclusions are drawn regarding the management of peat and excavated materials within the Site:

- As a result of the peat excavation and re-use estimates, it is demonstrated that all excavated peat can be suitably re-used on Site;
- Excavated peat will be used for the reinstatement of access track verges, cut and fill embankment slopes, reinstatement of turbine hardstandings, reinstatement of substation and compound areas, and in borrow pits following extraction;
- The estimates of excavated peat provided in this report are likely to be higher than actually occur, as micro-siting during construction will allow for the avoidance of localised pockets of deeper peat; and
- Sufficient methods have been defined to ensure that peat can be sensitively handled and stored on Site to allow for effective re-use.

## **APPENDIX A - FIGURES**



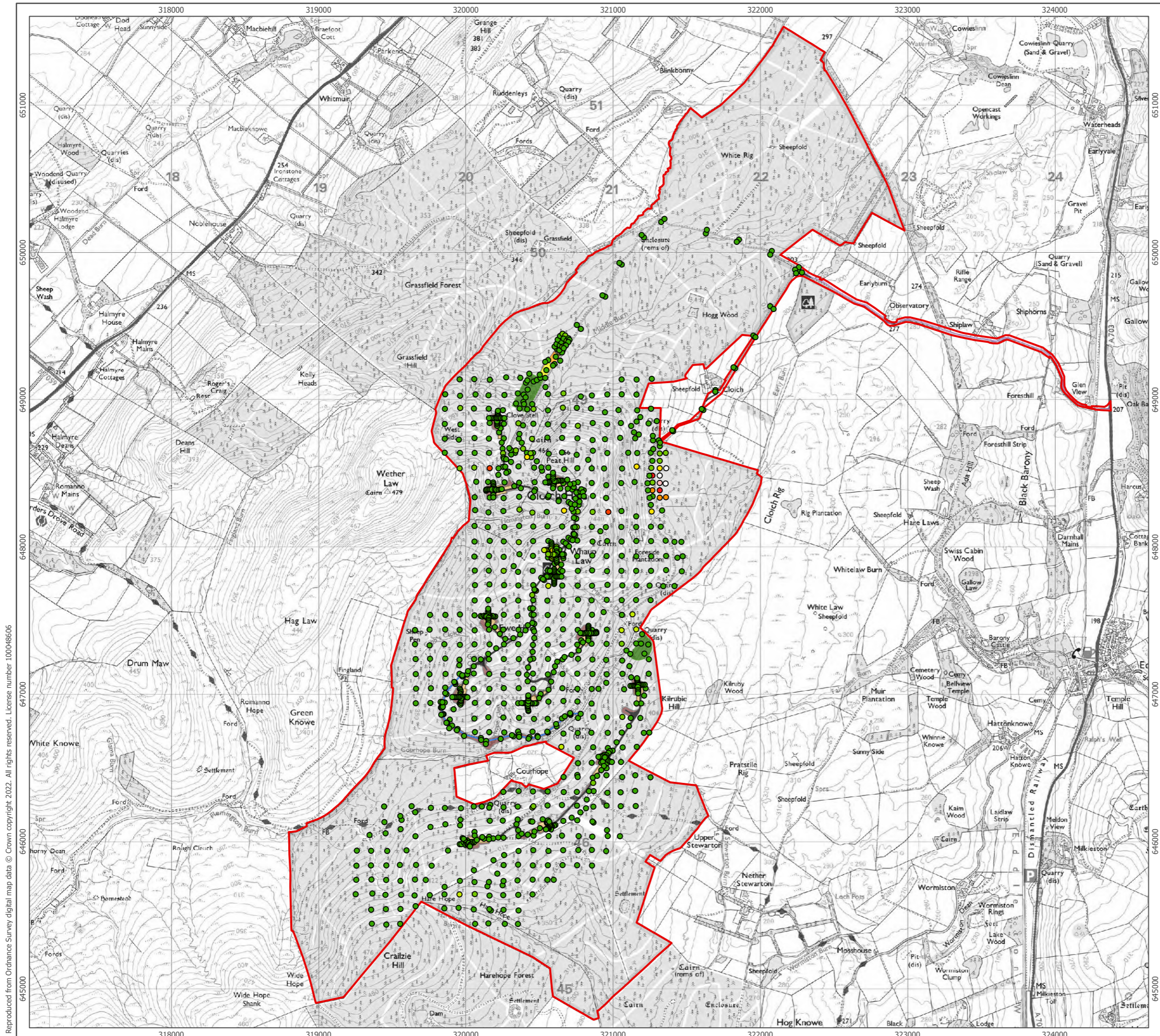
- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound

1:25,000 Scale @ A3  
  


Produced By: CS	Ref: 4519-REP-011
Checked By: DB	Date: 11/17/2022

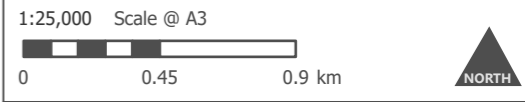
**Site Layout Plan**  
Figure 9.2.1

**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.2:**  
**Outline Peat Management Plan**



- Site Boundary
- Turbine Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound

- Peat Depth (m)**
- 0.00 - 0.50
  - 0.51 - 1.00
  - 1.01 - 1.50
  - 1.51 - 2.00
  - 2.01 - 2.50
  - 2.51 - 3.00
  - 3.01 - 3.50
  - 3.51 - 4.00
  - 4.01 +

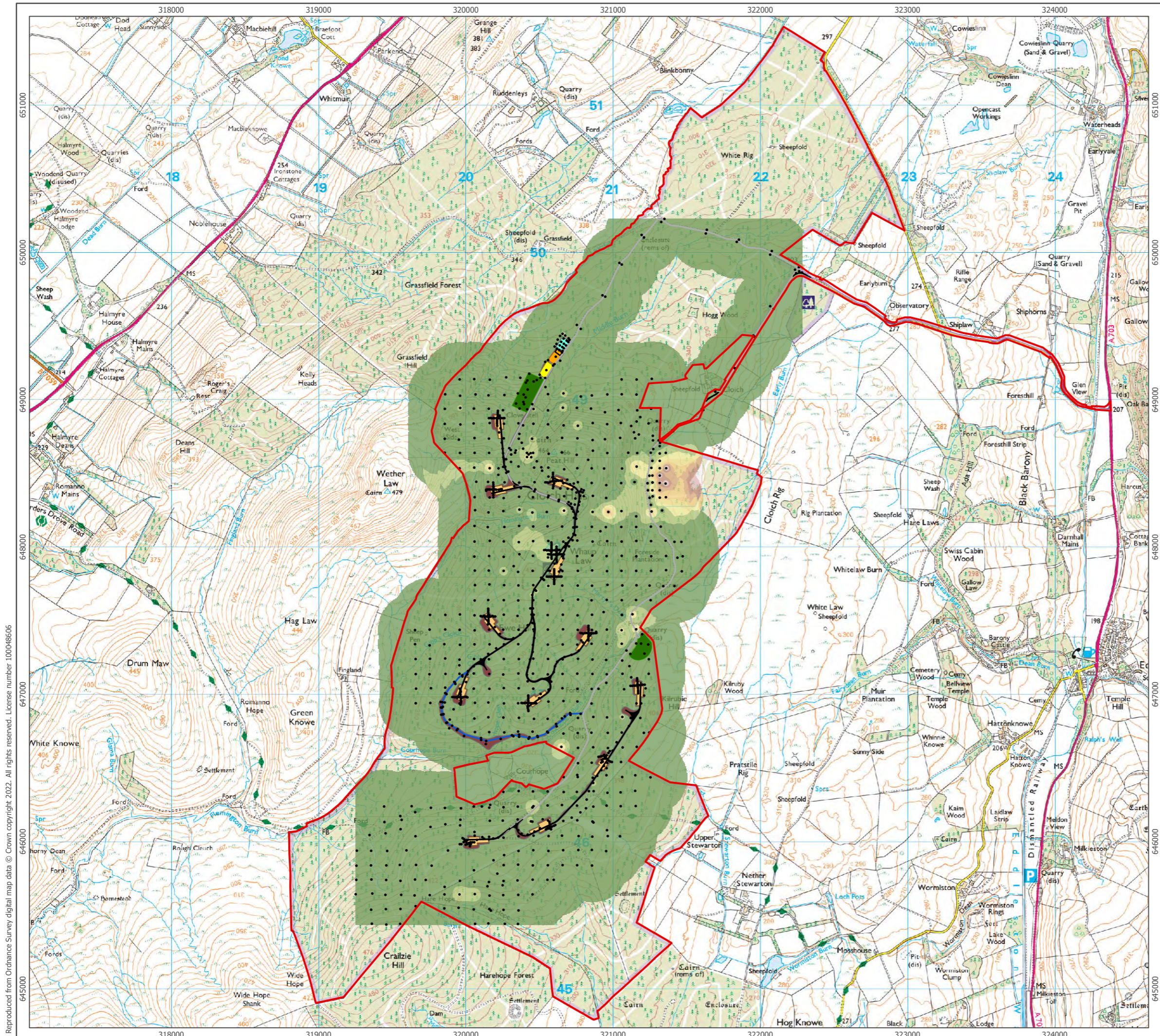


Produced By: CS	Ref: 4519-REP-012
Checked By: DB	Date: 11/17/2022

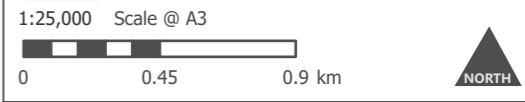
**Recorded Peat Depths**  
Figure 9.2.2

**Cloich Forest Wind farm SEI**  
**Technical Appendix 9.2:**  
**Outline Peat Management Plan**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606



- Site Boundary
- Peat Probe Locations
- Site Infrastructure**
- Borrow Pit
- Construction Compound
- Crane Hardstanding
- BESS Location
- Substation Compound
- New Access Track (Construction Traffic Only)
- New Access Track
- Existing Track (Subject to Localised Upgrades)
- Public Road
- Public Road Widening Works
- Earthworks
- SPT Temporary Construction Compound
- Peat Depths (m)**
- 0.00 - 0.50
- 0.51 - 1.00
- 1.01 - 1.50
- 1.51 - 2.00
- 2.01 - 2.50
- 2.51 - 3.00
- 3.01 - 3.50
- 3.51 - 4.00
- 4.01 +



Produced By: CS	Ref: 4519-REP-013
Checked By: DB	Date: 11/17/2022

**Interpolated Peat Depths**  
Figure 9.2.3

**Cloich Forest Wind Farm SEI**  
**Technical Appendix 9.2:**  
**Outline Peat Management Plan**

Reproduced from Ordnance Survey digital map data © Crown copyright 2022. All rights reserved. License number 100048606

## **APPENDIX B – CALCULATIONS**

**4519 -Cloich - Peat Excavation and Re-Use Calculations**

Infrastructure	Total Area of Infrastructure inc EW.	Peat Cut Volume	Total Acrotelm Excavation Est.	Total Catotelm Excavation Est.	Areas of Reinstament	Total Peat Re-use Est.	Total Acrotelm Re-use Est.	Total Catotelm Re-use Est.
<b>Turbines</b>								
T1	12580	1773	1773	0	7122	2008.4	2008.4	0
T2	10855	1768	1768	0	5397	1349.3	1349.3	0
T3	9052	2441	2441	0	3594	1073.5	1073.5	0
T4	10534	1755	1755	0	5076	1522.8	1522.8	0
T5	10226	2671	2671	0	4768	1430.4	1430.4	0
T6	13440	1828	1828	0	7982	2394.6	2394.6	0
T7	8477	822	822	0	3019	905.7	905.7	0
T8 (Revised Location)	7681	768	768	0	2223	666.9	666.9	0
T9	12484	1535	1535	0	7026	2107.8	2107.8	0
T10	10054	1694	1694	0	4596	1378.8	1378.8	0
T11	13976	1792	1792	0	8518	2555.4	2555.4	0
T12	9892	2199	2199	0	4434	1330.2	1330.2	0
<b>SUB-TOTAL</b>	<b>129251</b>	<b>21046</b>	<b>21046</b>	<b>0</b>	<b>63755</b>	<b>18723.8</b>	<b>18723.8</b>	<b>0</b>
<b>Tracks</b>								
New Tracks/PPs	89022	14028	14028	0	63022	18906.6	18906.6	0
Turning Heads	9799	2981	2981	0	6599	1979.7	1979.7	0
Tracks - Upgrade	24600	1230	1230	0	4100	1025	1025	0
<b>SUB-TOTAL</b>	<b>123421</b>	<b>18239</b>	<b>18239</b>	<b>0</b>	<b>73721</b>	<b>21911</b>	<b>21911</b>	<b>0</b>
<b>Construction Compound</b>								
WF Construction Compound	5674	453	453	0	5674	1418.5	1418.5	0
SST Construction Compound	5412	126	126	0	5412	1623.6	1623.6	0
<b>SUB-TOTAL</b>	<b>5412</b>	<b>579</b>	<b>579</b>	<b>0</b>	<b>5412</b>	<b>1623.6</b>	<b>1623.6</b>	<b>0</b>
<b>Substation</b>								
Substation Compound	5249	889	889	0	249	74.7	74.7	0
<b>SUB-TOTAL</b>	<b>5249</b>	<b>889</b>	<b>889</b>	<b>0</b>	<b>249</b>	<b>74.7</b>	<b>74.7</b>	<b>0</b>
<b>Borrow Pits</b>								
Borrow Pit 1	18610	2876	2876	0	18610	4652.5	4652.5	0
Borrow Pit 2	14399	2358	2358	0	14399	3599.75	3599.75	0
<b>SUB-TOTAL</b>	<b>33009</b>	<b>5234</b>	<b>5234</b>	<b>0</b>	<b>33009</b>	<b>8252.25</b>	<b>8252.25</b>	<b>0</b>
<b>TOTAL Excavation /Re-use Volume</b>		<b>45987</b>	<b>45987</b>	<b>0</b>	<b>176146</b>	<b>50586</b>	<b>50586</b>	<b>0</b>
. +10% contingency for Bullking		4599	4599	0				
<b>TOTAL Habitat Management - Peat Restoration and Ditch Blocking</b>						<b>0</b>	<b>0</b>	<b>0</b>
Deduction For floating Tracks						0	0	0
<b>SUB-TOTAL After Deduction</b>						<b>0</b>	<b>0</b>	<b>0</b>
<b>TOTAL PEAT EXCAVATION and REUSE</b>		<b>50586</b>	<b>50586</b>	<b>0</b>		<b>50586</b>	<b>50586</b>	<b>0</b>